-0009C

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SEE SHEET 3 FOR PLAN SHEET LAYOUT AT TIME OF INVESTIGATION **CONTENTS PROFILE** <u>LINE</u> <u>STATION</u> <u>PLAN</u> -Y2-98+85.00 TO 132+35.00 N/A 4-6 **CROSS SECTIONS** SHEETS LINE <u>STATION</u> -Y2-99+50 TO 133+50 7-46 **APPENDICES APPENDIX** <u>TITLE</u> <u>SHEETS</u> SOIL TEST RESULTS (I) 47-48 Α В GEOPHYSICAL TEST RESULTS 49-52

STATE OF NORTH CAROLINA

DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT

ROADWAY SUBSURFACE INVESTIGATION

COUNTY _GRAHAM

PROJECT DESCRIPTION MULTI-USE PATH ALONG NC 28 FROM SR 1238 (BILL CRISP RD) TO SR 1230 (HYDE TOWN RD)

INVENTORY

EFERENCE 2 N 5 S N m PROIEC

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	A-0009CE	1	52

CAUTION NOTICE

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOLI TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N.C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT 1999 107-6860. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

CENERAL SOL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU UN-PLACED TEST DATA CAN BE RELIED ON ONLY TO THE DECREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOLL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THES WATER LEVELS OR SOLL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

THE BIDDER OR CONTRACTOR IS CAUTIONED THAT DETAILS SHOWN ON THE SUBSURFACE PLANS ARE PRELIMINARY ONLY AND IN MANY CASES THE FINAL DESIGN DETAILS ARE DIFFERENT, FOR BIDDING AND CONSTRUCTION PURPOSES, REFER TO THE CONSTRUCTION PLANS AND DOCUMENTS FOR FINAL DESIGN INFORMATION ON THIS PROJECT. THE DEPARTMENT DOES NOT WARANT OR GUARANTE THE SUFFICIENCY OR ACCURACY OF THE INVESTIGATION MADE, NOR THE INTERPRETATIONS MADE, OR OPNION OF THE DEPARTMENT AS TO THE TYPE OF MATERIALS AND CONSTRUCTIONS TO BE ENCOUNTERED. THE BIDDER OR CONTRACTOR IS CAUTIONED TO MAKE SUCH INDEPENDENT SUBSURFACE INVESTIGATIONS AS HE DEEMS NECESSARY TO SATISFY HIMSELF AS TO CONDITIONS TO BE ENCOUNTERED ON THE PROJECT. THE CONTRACTOR SHALL HAVE NO CLAIM FOR ADDITIONAL COMPENSATION OR FOR AN EXTENSION OF TIME FOR ANY REASON RESULTING FROM THE ACTUAL CONDITIONS OR OF OR AN EXTENSION OF TIME FOR ANY REASON RESULTING FOR THE ACTUAL CONTINUONS ENCOUNTERED AT THE SITE DIFFERING FROM THOSE INDICATED IN THE SUBSURFACE INFORMATION.

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NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT SUBSURFACE INVESTIGATION

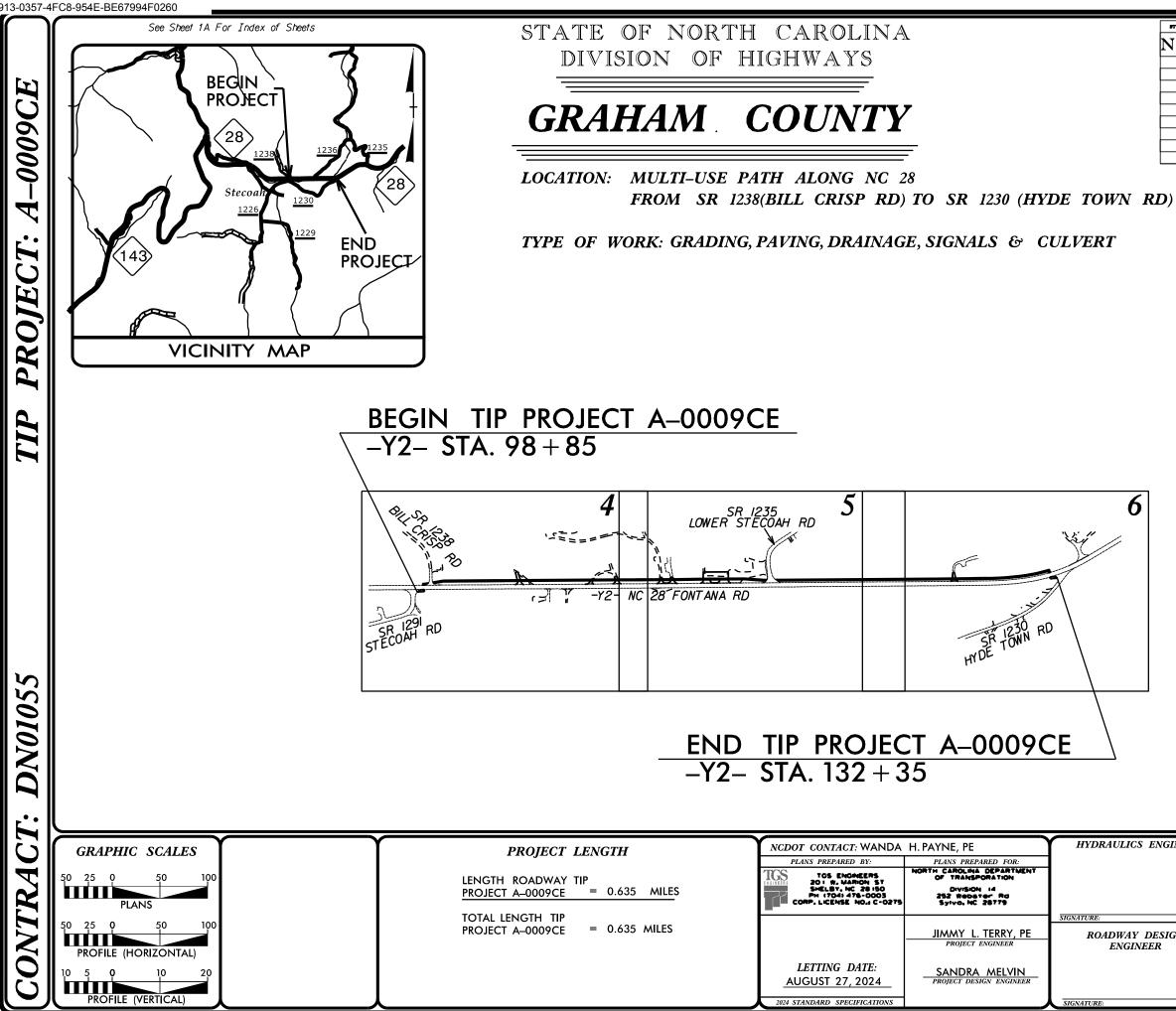
SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION	GRADATION	ROCK DESCRIPTION	TERMS AND DEFINITIONS
SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN	WELL GRADED-INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE.	HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL.	ALLUVIUM (ALLUV.)-SOILS THAT HAVE BEEN TRANSPORTED BY WATER.
BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION	UNIFORMLY GRADED-INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE. GAP-GRADED-INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.	SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60	ADUIFER-A WATER BEARING FORMATION OR STRATA.
IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH	ANGULARITY OF GRAINS	BLOWS IN NON-COASTAL PLAIN MATERIAL, THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK.	ARENACEOUS-APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.
AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE,	THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS:	ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:	ARGILLACEOUS-APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING
VERY STIFF.GRAY.SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6	ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.	WEATHERED NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES >	A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.
SOIL LEGEND AND AASHTO CLASSIFICATION	MINERALOGICAL COMPOSITION	ROCK (WR) 100 BLOWS PER FOOT IF TESTED.	ARTESIAN-GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND
GENERAL GRANULAR MATERIALS SILT-CLAY MATERIALS ORGANIC MATERIALS CLASS. (≤ 35% PASSING 200) (> 35% PASSING 200) ORGANIC MATERIALS	MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC.	CRYSTALLINE ROCK (CR) FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE,	SURFACE.
GROUP A-1 A-3 A-2 A-4 A-5 A-6 A-7 A-1, A-2 A-4, A-5	ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.		CALCAREOUS (CALC.)-SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.
CLASS. A-1-a A-1-b A-2-4 A-2-5 A-2-6 A-2-7 A-7-5 A-3 A-6, A-7		NUN-CHISTALLINE	COLLUVIUM-ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM
SYMBOL SYMBOL	SLIGHTLY COMPRESSIBLE LL < 31 MODERATELY COMPRESSIBLE LL = 31-50	COASTAL PLAIN COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD	OF SLOPE.
7. PASSING	HIGHLY COMPRESSIBLE LL > 50	SEDIMENTARY ROCK SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED	CORE RECOVERY (REC.)-TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
*10 50 MX *40 30 MX 50 MX 51 MN S012 GRANULAR S012 GRANULAR CLAY MUCK, S012 CONTRACT S012 CLAY PEAT	PERCENTAGE OF MATERIAL	WEATHERING	DIKE-A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT
280 15 MX 25 MX 10 MX 35 MX 35 MX 35 MX 35 MX 36 MN 36 MN 36 MN 36 MN 36 MN	GRANULAR SILT-CLAY ORGANIC MATERIAL SOILS OTHER MATERIAL	FRESH ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER	ROCKS OR CUTS MASSIVE ROCK.
MATERIAL	TRACE OF ORGANIC MATTER 2-3% 3-5% TRACE 1-10%	HAMMER IF CRYSTALLINE.	DIP-THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.
PASSING *40	LITTLE ORGANIC MATTER 3-5% 5-12% LITTLE 10-20% MODERATELY ORGANIC 5-10% 12-20% SOME 20-35%	VERY SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN,	DIP DIRECTION (DIP AZIMUTH)-THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE
PI 6 MX NP 10 MX 10 MX 11 MN 11 MN 10 MX 10 MX 11 MN 11 MN 11 MN MODERATE HIGHLY	HIGHLY ORGANIC > 10% > 20% HIGHLY 35% AND ABOVE	(V SLI.) CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.	LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.
GROUP INDEX 0 0 0 4 MX 8 MX 12 MX 16 MX NO MX AMOUNTS OF URDANIL	GROUND WATER	SLIGHT ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO	FAULT-A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE
USUAL TYPES STORE FRAGS. EINE STITY OF CLAVEY STITY CLAVEY MATTER	✓ WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING	(SLI.) 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR	SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.
OF MAJOR GRAVEL AND SAND GRAVEL AND SAND SOILS SOILS	STATIC WATER LEVEL AFTER <u>24</u> HOURS	CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS. MODERATE SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN	FISSILE-A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES. FLOAT-ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM
		(MOD.) GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY, ROCK HAS	PARENT MATERIAL.
AS SUBGRADE EXCELLENT TO GOOD FAIR TO POOR POOR UNSUITABLE		DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.	FLOOD PLAIN (FP)-LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.
PI OF A-7-5 SUBGROUP 195 LL-30 ; PI OF A-7-6 SUBGROUP IS > LL-30	- O-M- Spring or seep	MODERATELY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL	FORMATION (FM.)-A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE
CONSISTENCY OR DENSENESS	MISCELLANEOUS SYMBOLS	SEVERE AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH	FIELD.
COMPACTNESS OR RANGE OF STANDARD RANGE OF UNCONFINED		(MOD.SEV.) AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. IF TESTED, WOULD YIELD SPT REFUSAL	JOINT-FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.
PRIMARY SOIL TYPE CONFIGURESS ON PENETRATION RESISTENCE COMPRESSIVE STRENGTH (N-VALUE) (TONS/FT ²)	WITH SOIL DESCRIPTION OF ROCK STRUCTURES	SEVERE ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT	LEDGE-A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.
GENERALLY VERY LOOSE < 4	SOIL SYMBOL	(SEV.) REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED	LENS-A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.
OLICIAL LOOSE 4 TO 10 GRANULAR MEDIUM DENSE 10 TO 30 N/A		TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. <u>IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF</u>	MOTTLED (MOT.)-IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS
MATERIAL DENSE 30 TO 50	ARTIFICIAL FILL (AF) OTHER AUGER BORING CONE PENETROMETER	VERY ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE	USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.
VERY DENSE > 50		SEVERE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK	PERCHED WATER-WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.
VERY SOFT < 2 < 0.25 GENERALLY SOFT 2 TO 4 0.25 TO 0.5	INFERRED SOIL BOUNDARY	(V SEV.) REMAINING, SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <u>IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF</u>	RESIDUAL (RES.) SOIL-SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.
SILT-CLAY MEDIUM STIFF 4 TO 8 0.5 TO 1.0	TIST BORING WITH CORE	COMPLETE ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND	ROCK QUALITY DESIGNATION (ROD)-A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF
MATERIAL STIFF 8 T0 15 1 T0 2 (COHESIVE) VERY STIFF 15 T0 30 2 T0 4		SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.	ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE
HARD > 30 > 4	TTTTT ALLUVIAL SOIL BOUNDARY ALLUVIAL SOIL BOUNDARY INSTALLATION SPT N-VALUE		RUN AND EXPRESSED AS A PERCENTAGE.
TEXTURE OR GRAIN SIZE	RECOMMENDATION SYMBOLS		SAPROLITE (SAP.)-RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.
U.S. STD. SIEVE SIZE 4 10 40 60 200 270		VERY HARD CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REOUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.	SILL-AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND
DPENING (MM) 4.76 2.00 0.42 0.25 0.075 0.053		HARD CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED	RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO
BOULDER COBBLE GRAVEL COARSE FINE SILT CLAY	SHALLOW UNCLASSIFIED EXCAVATION - USED IN THE TUP 3 FEEL OF UNDERCUT ACCEPTABLE DEGRADABLE ROCK EMBANKMENT OR BACKFILL	TO DETACH HAND SPECIMEN.	THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.
(BLDR.) (COB.) (GR.) (SL.) (CSE. SD.) (F SD.) (SL.) (CL.)	ABBREVIATIONS	MODERATELY CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE HARD EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED	SLICKENSIDE-POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.
GRAIN MM 305 75 2.0 0.25 0.05 0.005	AR-AUGER REFUSAL MEDMEDIUM VST-VANE SHEAR TEST	BY MODERATE BLOWS.	STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT)-NUMBER OF BLOWS (N OR BPF) OF
SIZE IN. 12 3	BT-BORING TERMINATED MICAMICACEOUS WEAWEATHERED	MEDIUM CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT.	A 140 LB.HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL
SOIL MOISTURE-CORRELATION OF TERMS	CLCLAY MODMODERATELY γ - UNIT WEIGHT CPT-CONE PENETRATION TEST NP-NON PLASTIC γ_{d} - DRY UNIT WEIGHT	HARD CAN BE EXCAVATED IN SMALL CHIPS TO PEICES I INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.	TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.
SOIL MOISTURE SCALE FIELD MOISTURE GUIDE FOR FIELD MOISTURE DESCRIPTION	CSECOARSE ORGORGANIC	SOFT CAN BE GROVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS	STRATA CORE RECOVERY (SREC.)-TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY
(ATTERBERG LIMITS) DESCRIPTION BOIDE FOR FIELD MOISTORE DESCRIPTION	DMT-DILATOMETER TEST PMT-PRESSUREMETER TEST <u>SAMPLE ABBREVIATIONS</u> DPT-DYNAMIC PENETRATION TEST SAPSAPROLITIC S-BULK	FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.	TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.
- SATURATED - USUALLY LIQUID; VERY WET, USUALLY	e - VOID RATIO SDSAND, SANDY SS-SPLIT SPOON	VERY CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH	STRATA ROCK QUALITY DESIGNATION (SROD)-A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY
(SAT.) FROM BELOW THE GROUND WATER TABLE	F-FINE SLSILT, SILTY ST-SHELBY TUBE FOSSFOSSILIFEROUS SLISLIGHTLY RS-ROCK	SOFT OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY	THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.
	FRACFRACTURED, FRACTURES TCR-TRICONE REFUSAL RT-RECOMPACTED TRIAXIAL	FINGERNAIL.	TOPSOIL (TS.)-SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.
RANGE - WET-(W) ATTAIN OPTIMUM MOISTURE	FRAGSFRAGMENTS W-MOISTURE CONTENT CBR-CALIFORNIA BEARING HIHIGHLY V-VERY RATIO	FRACTURE SPACING BEDDING	BENCH MARK: N/A
	EQUIPMENT USED ON SUBJECT PROJECT	TERM SPACING TERM THICKNESS VERY WIDE MORE THAN 10 FEET VERY THICKLY BEDDED 4 FEET	
OM _ OPTIMUM MOISTURE - MOIST-(M) SOLID; AT OR NEAR OPTIMUM MOISTURE	DRILL UNITS: ADVANCING TOOLS: HAMMER TYPE:	WIDE 3 TO 10 FEET THICKLY BEDDED 1.5-4 FEET	ELEVATION: FEET
SL SHRINKAGE LIMIT		MODERATELY CLOSE 1 TO 3 FEET THINLY BEDDED 0.16-1.5 FEET CLOSE 0.16 TO 1 FOOT VERY THINLY BEDDED 0.03-0.16 FEET	NOTES:
- DRY-(D) REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE		VERY CLOSE LESS THAN 0.16 FEET THICKLY LAMINATED 0.008-0.03 FEET	ROADWAY DESIGN FILES DATED 05/02/24 PROVIDED BY TGS ENGINEERS
	CME-550	THINLY LAMINATED < 0.008 FEET	
PLASTICITY		INDURH I ION FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.	SOIL, WEATHERED ROCK, AND CRYSTALLINE ROCK LINES ARE BASED ON AN INTERPRETATION OF BORE HOLE AND SEISMIC REFRACTION
PLASTICITY INDEX (PI) DRY STRENGTH	X CME-550X HARD FACED FINGER BITS	PURPING WITH FINGER EDEES NUMEROUS CRAINS.	DATA AND SHALL BE CONSIDERED AS APPROXIMATE.
NON PLASTIC Ø-5 VERY LOW SLIGHTLY PLASTIC 6-15 SLIGHT	VANE SHEAR TEST	FRIABLE GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.	
MODERATELY PLASTIC 16-25 MEDIUM HIGHLY PLASTIC 26 OR MORE HIGH	CASING W/ ADVANCER	MODERATELY INDURATED GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE:	
		BREAKS EASILY WHEN HIT WITH HAMMER.	
COLOR	X DIEDRICH D50	INDURATED GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE: DIFFICULT TO BREAK WITH HAMMER.	
DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY).	CORE BIT	CHARP HAMMER RI OWS RECHTRED TO RREAK SAMPLE.	
MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.		EXTREMELY INDURATED SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.	DATE: 8-15-14
			8

PROJECT REFERENCE NO.

A-0009CE

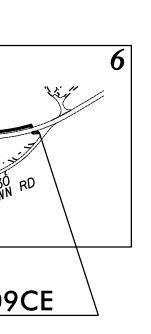
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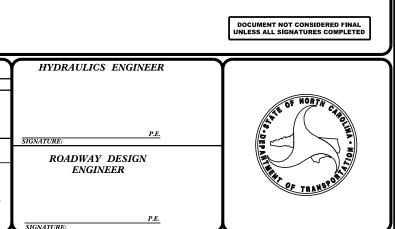


NCDOT CONTACT: WANDA H. PAYNE, PE PLANS PREPARED FOR: TH CAROLINA DEPARTMENT OF TRANSPORATION PLANS PREPARED BY: TOS ENGINEERS 20 I W. MARION ST SHELBY, NC 28 ISO PH (704) 476-0003 CORP. LICENSE NO.1 C-02 DIVISION 14 252 Webster Ro Sylvo, NC 28779 JIMMY L. TERRY, PE PROJECT ENGINEER LETTING DATE: SANDRA MELVIN AUGUST 27, 2024

5

STATE	STATE PROJECT REPERENCE NO.		SHEET NO.	TOTAL SHEETS	
N.C.	A-0009CE			3	
STAT	E PROJ. NO.	F. A. PROL NO.		DESCRIPT	TON
3257	72.3.20			CON	ST





NAD 83/2011

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5/24/2024

STATE PROJECT:	35272.3.20
TIP NUMBER:	A-0009CE
F/A NUMBER:	N/A
COUNTY:	GRAHAM
DESCRIPTION:	Multi-Use Path Along NC 28 from SR 1238 (Bill Crisp Rd) to SR 1230 (Hyde Town Rd)

SUBJECT: Geotechnical Roadway Inventory Report

PROJECT DESCRIPTION

This roadway widening project consists of improvements NC 28 between SR 1238 (Bill Crisp Rd) and SR 1230 (Hyde Town Rd). The project is approximately 0.633 miles in length, measured along -Y2- (NC 28) from Station 98+85 to 132+35. The construction consists of the addition of a multi-use path adjacent to -Y2- and a reinforced concrete culverts extension, and associated infrastructure. The project alignment is not located entirely within NCDOT right-of-way. The following alignments are included as part of this investigation:

<u>Alignment</u>	<u>Stations</u>	<u>TIP No.</u>
-Y2- (NC 28)	98+85 to 132+35	A-0009CE

Some boring locations were planned in archeologically sensitive areas; however, these areas could not be accessed at the time of the investigation and were excluded.

The following culverts are included as part of this investigation:

<u>Culvert</u>	Stations (Alignment)
Structure over Edwards Branch	99+82 (-Y2-)

The following cut slopes oriented steeper than 2:1 (H:V) but flatter than 1.5:1 (H:V) are included as part of this investigation:

Stations (Alignment)	<u>Offset</u>
101+00 to 102+50 (-Y2-)	LT
104+50 to 106+50 (-Y2-)	LT

All other project slopes are 2:1 (H:V) or flatter.

The project alignment is generally located in a rural area with existing grades ranging from relatively flat along the west of the project, becoming more mountainous along the central and eastern areas of the alignment. Due to the variation of existing conditions and proposed construction across the project alignment, the project has been divided into sections to describe the change in grades and proposed construction in a more descriptive manner.

This section of the project extends through the floodplain of Stecoah Creek, with generally steep slopes on the left side of the alignment and moderate fills on the right side where the route runs adjacent to Stecoah Creek. Numerous borings

throughout this section encountered alluvial soils within the proposed roadway (reference Areas of Special Geotechnical Interest in this report).

The geotechnical field investigation was conducted by CG2 during the period of May 2021 through December 2021. The investigation was performed in several phases due to project schedule and other demands which required moving equipment to various sections of the project. Subcontracted drill crews were used to drill, sample, and log 41 of the borings in this report. The drill rigs used were ATV-mounted CME 550X and a track-mounted Diedrich D-50 equipped with automatic hammers. Standard Penetration Tests were performed at selected depths for the 41 borings. Additionally, some areas could not be accessed by the drilling equipment, and the presence of boulders and cobbles prevented obtaining subsurface information using hand sampling methods. In these instances, field staff visually identified areas of interest. Representative soil samples were collected for visual-manual classification in the field and selected samples were submitted for laboratory analysis by an approved NCDOT M&T testing facility.

Due to site constraints, archeologically sensitive areas, and stakeholder limitations, select areas were inaccessible to drilling equipment. As such, CG2 subcontracted GEL Solutions (GEL) to perform a seismic refraction investigation at various areas across the project alignment between May and September 2021. GEL performed 3 seismic refraction lines utilizing a Geometrics Geode Seismograph with up to 24 vertical geophones with a 16-pound sledgehammer as an energy source. The purpose of the seismic refraction investigation was to assist in estimating the top of weathered rock and/or bedrock which may affect the proposed construction. CG2 interpreted the top of weathered rock based on a compressional wave velocity (Vp) of 4,500 ft/sec and the top of bedrock based on a Vp of 7,500 ft/sec.

PHYSIOGRAPHY AND GEOLOGY

The project alignment is located within the Blue Ridge Physiographic Province of North Carolina (Blue Ridge). In general, the project alignments topography is consistent with the Blue Ridge, having rolling terrain that is moderately wooded with intermittent mountainous slopes and ridges at variable distances along the alignment. Towards the east along NC 28 (-Y2-), floodplains and stream terraces are present paralleling the existing roadways.

According to the geologic map and associated data of southwestern North Carolina from Weiner & Merschat, 1992, the project alignment mostly lies within the Murphy Syncline, a northeast-southwest trending trough fold. This now-tilted u-shaped fold has experienced multiple regional deformational events, which have overprinted the older synclinal fold with more recent foliations, faulting, and open folds. These geologic events have resulted in low to medium grade metamorphic rock (chlorite to kyanite facies). The project alignment is underlain by the Anakeesta (Wehutty) and stratigraphically overlying Ammons Formations. The bedrock under the site consists of meta-sedimentary rock including interlayers of Phyllite, Argillite, Schist, Meta-Sandstone, Meta-Siltstone, and Meta-Graywacke, and Marble of the Anakeesta (Wehutty) Formations. (Reference "Geological Investigation of A-9 A, B, & C (Stecoah and Tatham Gaps)" prepared by Acker & Reed, December 5, 1995). The rock encountered during this investigation was classified as Meta-Graywacke, Meta-Siltstone, and Meta-Siltstone, and Meta-Siltstone, and Meta-Siltstone, and Meta-Siltstone, Meta-Siltstone, Meta-Siltstone, Meta-Siltstone, Meta-Siltstone, Meta-Siltstone, Meta-Siltstone, Stere & Reed, December 5, 1995). The rock encountered during this investigation was classified as Meta-Graywacke, Meta-Siltstone, and Meta-Sandstone, Mica Schist, and Schist.

Based on a review of the February 29, 2009 "Acid Producing (Hot Rock) Investigation and Potential Along Proposed Corridor" prepared by NCDOT and our experience in this region, rock with the potential to produce acidic runoff upon exposure to air and water (hot rock) may be found within the Ammons Formation and members, namely the Horse Branch Member, and the Anakeesta (Wehutty) Formation. Hot rock of the Nantahala Formation may also produce acidic conditions; however, the current proposed alignment does not appear to extend to areas underlain by this formation. As these geologic formations are known to be acid-producing, CG2 subcontracted HDR Engineering, Inc. of the Carolinas to investigate the risk for acidic potential to the project site and, if necessary, prepare a safety protocol for the handling,

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treatment, and disposal of the hot rock particular to this project site ("Final Rock Slope Design" dated February 25, 2022). The evaluation consisted of twenty hand samples collected by CG2 (tested for Net Neutralization Potential (NNP)), twenty rock core samples, and three split spoon samples from boreholes to investigate three proposed rock cuts along NC 28 (-Y2-) for Acid-Base Testing. We concur with the referenced report prepared by HDR, that acid-producing rock in the project area does not appear to pose a significant risk along NC 28 (-Y2-) routed through the proposed alignment.

Within the project alignment, much of the bedrock is overlain by near-surface material consisting of residual soil and transported soil deposits of varying ages. Residual soils are derived from in situ chemical and physical weathering of the rocks in the area. The residual soils in this region are typically more fine grained with a higher clay content near the surface due to advanced weathering, and typically become more coarse grained with increasing depth as the degree of weathering decreases. As the degree of weathering decreases, the residual soils generally retain the overall appearance and fabric of the parent rock (sometimes referred to as "saprolite"). The boundary between soil and rock is not always sharply defined. A transitional zone termed "weathered rock" is often found overlying the parent bedrock. Weathered rock is defined as material requiring 100 blows with less than one foot of penetration from the SPT hammer.

Transported soils within the project alignment consist of alluvial (water-transported) and colluvial (gravity-transported) deposits of varying ages. Alluvial soil deposits are primarily from Sweetwater Creek and several other smaller creeks and streams present within the project alignment. Some streams and creeks are the byproducts of numerous springs located throughout the project corridor. Older, weathered alluvial deposits were also encountered and are referred to as fans or stream terraces. In areas immediately adjacent to existing waterways, younger alluvial deposits (floodplain soils) were encountered at lower elevations than terrace deposits or residual soils.

Colluvial soil deposits were observed within portions of the project alignment on slopes and/or at the base of slopes and ridges. Colluvial soils deposits are typically the result of mass soil movement and long-term soil creep which are common in this geographical area at the base of hills, slopes, and mountain ridges.

SOIL PROPERTIES

Soils and rock encountered during this investigation include roadway embankment, artificial fill, alluvial, colluvial, residual, weathered rock, and crystalline rock.

Organic topsoil was encountered in some borings at the ground surface up to approximately 0.5 feet below the existing ground surface.

Roadway Embankment soils are similar in nature to residual soils and may be derived from nearby sources. The finegrained roadway embankment soils consist of very soft to hard, sandy silt (A-4), sandy, clayey silt (A-5), sandy clay (A-6), and sandy, silty clay (A-7), with trace to little gravel and trace organics. The coarse-grained soils encountered consist of very loose to very dense, sandy gravel (A-1-a), silty, gravelly sand (A-1-b), and silty sand (A-2-4), with trace to little gravel and trace organics.

Artificial Fill soils are materials that have been moved and/or placed by man or mechanical means. The artificial fill soils encountered consist of very loose to dense silty, sand (A-2-4) and soft to hard, sandy silt (A-4), sandy, clayey silt (A-5), and fine sandy clay (A-7), 6ith trace to little gravel and organics. The soils appeared to be sourced locally.

Alluvial soils are materials transported by water and are typically found in floodplains and stream terrace environments. The fine-grained alluvial soils consist of very soft to hard, sandy silt (A-4), sandy, clayey silt (A-5), sandy, silty clay (A-7), with trace to little gravel and cobbles and organics and trace mica. The coarse-grained soils encountered consist of very

loose to very dense, sandy gravel (A-1-a), gravelly, silty sand (A-1-b), and silty sand (A-2-4), with little gravel. Alluvial boulders were also encountered infrequently across the project.

Colluvial soils were encountered as semi-consolidated soil deposits beneath existing embankments and unconsolidated soils deposited at the base of hillsides by creep and/or water flow. Colluvial soils were not encountered in the project borings, however, these soils may be encountered in areas in proximity to steep slopes and in valleys.

Residual soils are derived from the weathering of underlying rock in the area. The residual fine-grained soils consist of soft to hard, slightly plastic sandy silt (A-4), sandy, clayey silt (A-5), sandy clay (A-6), and sandy, silty clay (A-7-5/6), with trace mica, organics, and manganese oxide and trace to little gravel-sized rock fragments. The coarse-grained soils consist of very loose to very dense, sandy gravel (A-1-a), silty, gravelly sand (A-1-b), and silty sand (A-2-4), with trace mica and manganese oxide and trace to little gravel-sized rock fragments.

Weathered rock was also encountered along the project alignment within 7 borings. The weathered rock encountered consists of Schist and Meta-Sandstone. The top of weathered rock was encountered at depths ranging from approximately 3 to 38.5 feet below the existing ground surface.

Crystalline rock was encountered along the project alignment within two of the borings. These two borings were terminated on crystalline rock. The crystalline rock encountered was classified as Schist and Meta-Sandstone was encountered at depths ranging from approximately 4.3 to 13.0 feet below the existing ground surface. For borings terminated on crystalline rock where rock was not recovered, the rock was classified either based on materials recovered within the boring or on proximal rock outcrop type.

GROUNDWATER

Groundwater measurements were taken between the months of May to December 2021. Groundwater measurements were attempted at the completion of drilling in each boring, at which time groundwater was encountered in 25 borings at depths ranging from approximately 4.0 to 26.5 feet below the existing ground surface. Subsequent groundwater measurements were attempted after at least 24 hours following the completion of drilling, at which time groundwater was encountered in 29 of the borings at depths ranging from approximately 2.5 feet to 21.2 feet below the existing ground surface. Three of the borings were backfilled immediately upon completion of drilling activities for safety reasons or at the request of a property owner. The remaining borings were recorded as dry at the bottom of the boring cylinder. Groundwater is expected to impact construction. The soils encountered were generally described as moist to wet above the groundwater elevation and moist to saturated below groundwater elevation.

Water wells were encountered within the project alignment. Water wells could be encountered at other locations due to the presence of dwellings and businesses.

<u>Alignment</u>	<u>Stations</u>
-Y2-	89+57
-Y2-	95+33

Springs and seeps were encountered within the project alignment at the following locations:

<u>Type</u>	<u>Alignment</u>	<u>Stations</u>	<u>Offsets (ft)</u>
Spring	-Y2-	111+80	215 LT

<u>Offsets (ft)</u> 172 LT 118 RT Docusign Envelope ID: 93A88913-0357-4FC8-954E-BE67994F0260



AREAS OF SPECIAL GEOTECHNICAL INTEREST

The following borehole locations encountered very soft to soft or very loose to loose soils which have the potential to cause embankment stability and/or long-term settlement problems:

<u>Alignment</u>	<u>Stations</u>	Offsets (ft)
-Y2-	99+97	7 RT
-Y2-	103+48 to 105+65	47 LT to 3 RT
-Y2-	107+75 to 113+50	3 RT to 35 RT
-Y2-	116+92 to 122+98	31 LT to 34 RT
-Y2-	124+99 to 127+40	19 LT to 34 RT
-Y2-	129+47 to 133+13	19 LT

Highly Plastic Soils: Highly plastic soils (PI > 25) were not encountered in the borings on the project.

Shallow groundwater was encountered within 6 feet of proposed subgrade at the following borehole locations:

<u>Alignment</u>	<u>Stations</u>	Offsets (ft)
-Y2-	124+01 to 124+99	31 RT to 32 RT
-Y2-	125+96 to 126+88	33 RT to 34 RT
-Y2-	128+01	32 RT

In addition, shallow groundwater may be encountered within 3 feet of the existing ground at the following locations:

<u>Alignment</u>	<u>Stations</u>	Offsets (ft)
-Y2-	108+75 to 109+50	35 RT
-Y2-	110+93	3 RT
-Y2-	121+13	31 LT
-Y2-	126+88	33 RT
Y2-	128+01	32 RT
-Y2-	129+01 to 129+47	37 LT to 19 LT

Alluvial soils were encountered on the project at the following borehole locations:

<u>Alignment</u>	<u>Stations</u>	<u>Offsets (ft)</u>
-Y2-	99+97	7 RT
-Y2-	107+75 to 118+01	10 LT to 35 RT
-Y2-	119+03	33 RT
-Y2-	122+03	31 RT
-Y2-	128+01 to 129+00	25 LT to 35 RT
-Y2-	129+47	19 LT

Artificial Fill soils were encountered on the project at the following borehole locations:

<u>Alignment</u>	<u>Stations</u>	<u>Offsets (ft)</u>
-Y2-	103+48	1 RT

Colluvial soils may be detrimental to the proposed improvements due to variable consistency and character of these soils. Colluvial soils often contain deleterious materials such as boulders, gravel, organics, loose/soft soils, and can become unstable during or after construction. Colluvial soils present significant risk if they become saturated or are left exposed to continued water infiltration which may cause previously stable colluvial soils to creep, slide, or become unstable. Colluvial soils were not encountered on the project boreholes but may be present on the project.

Rock was not encountered within 6 feet of the proposed cut elevation at the following borehole and/or seismic refraction investigation locations.

For rock locations in other areas on the project, please see the previously referenced reports prepared by HDR.

Ponds were observed in the vicinity of the project limits at the following locations:

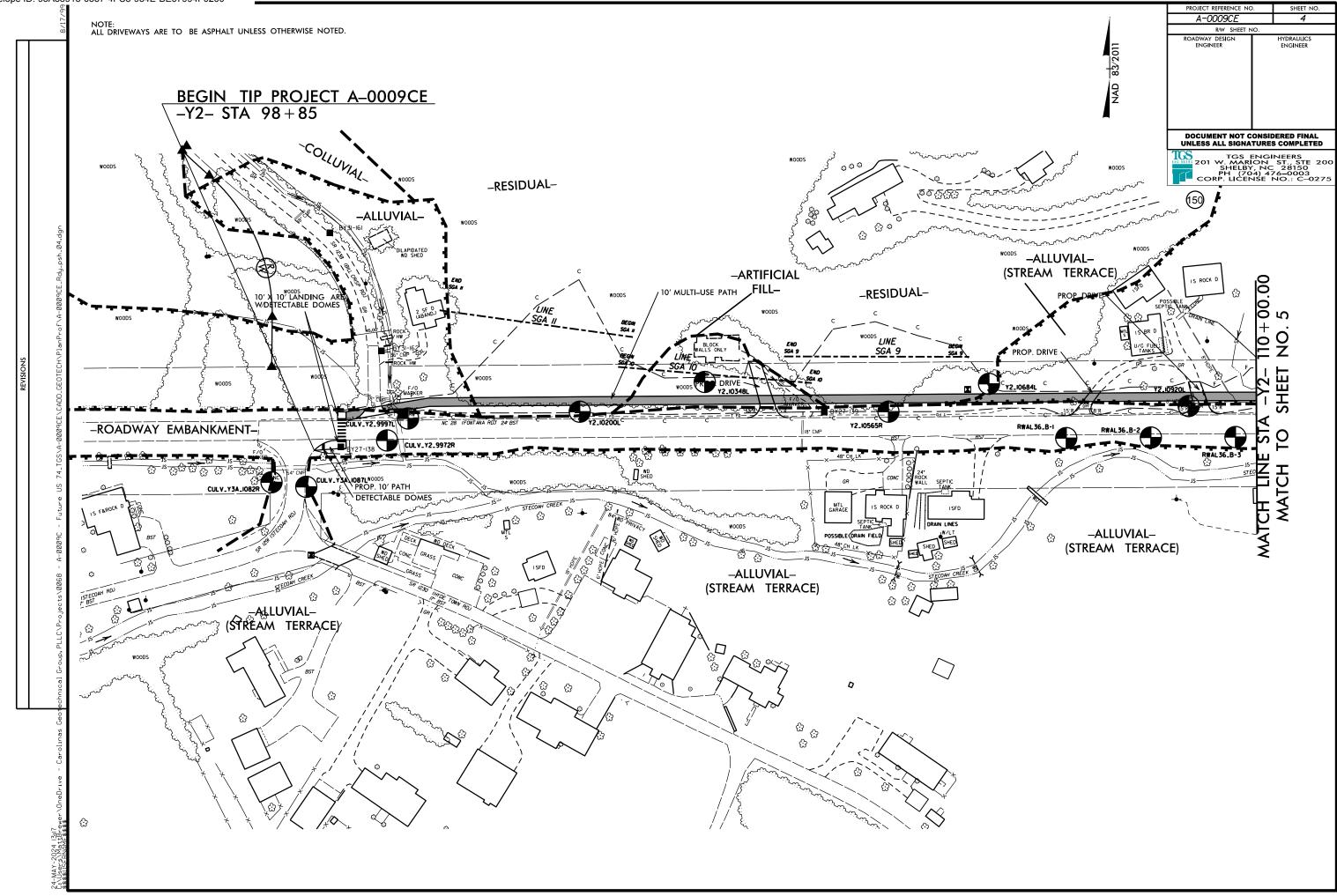
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-Y2-	88+40 to 89+00	RT
-Y2-	118+50 to 123+75	LT

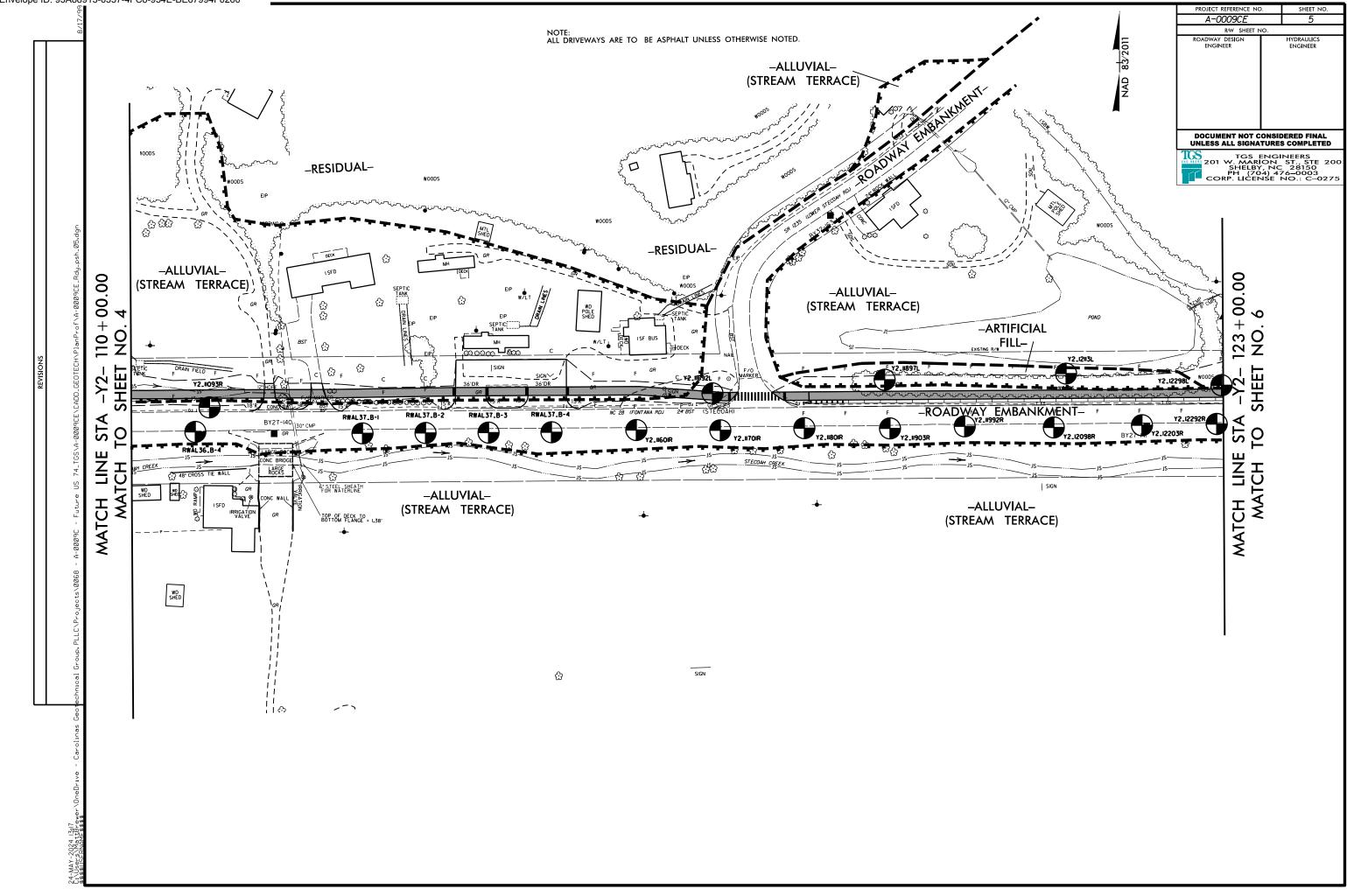
GEOTECHNICAL TESTING

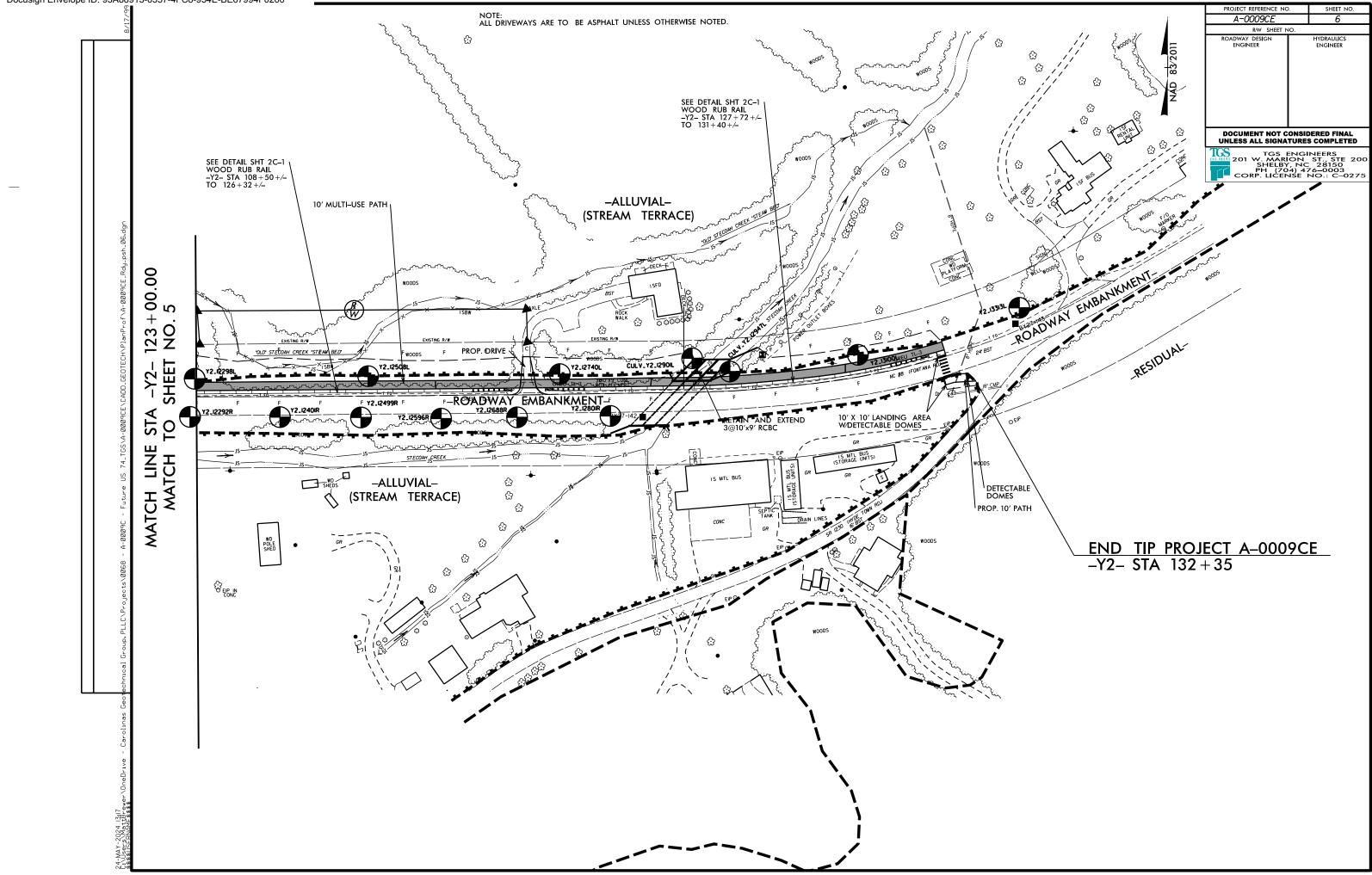
Split spoon samples were selected for laboratory testing including Atterberg limits, grain size distribution analysis with hydrometer, and natural moisture.

Sincerely, Carolinas Geotechnical Group, PLLC

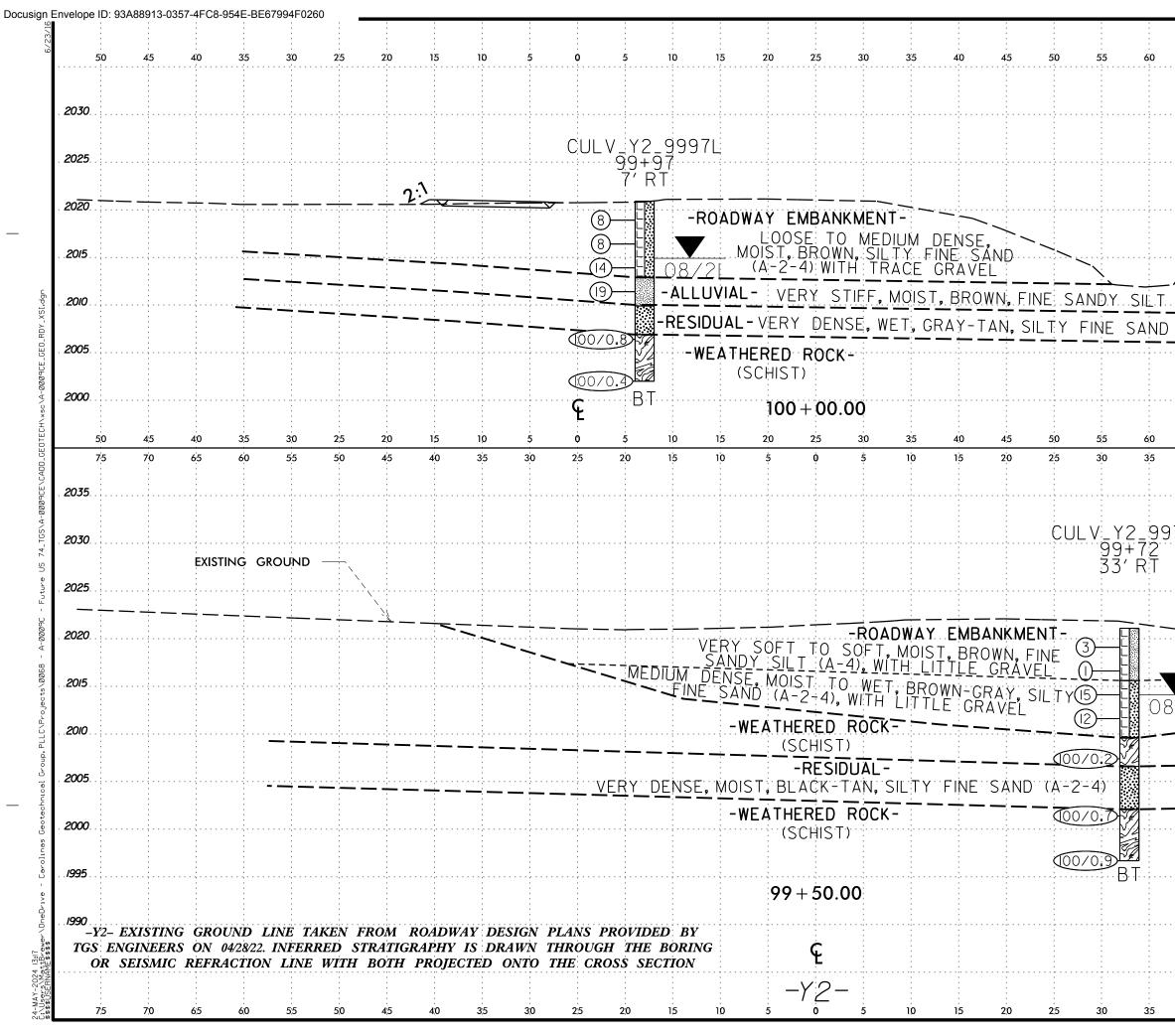
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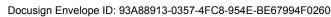


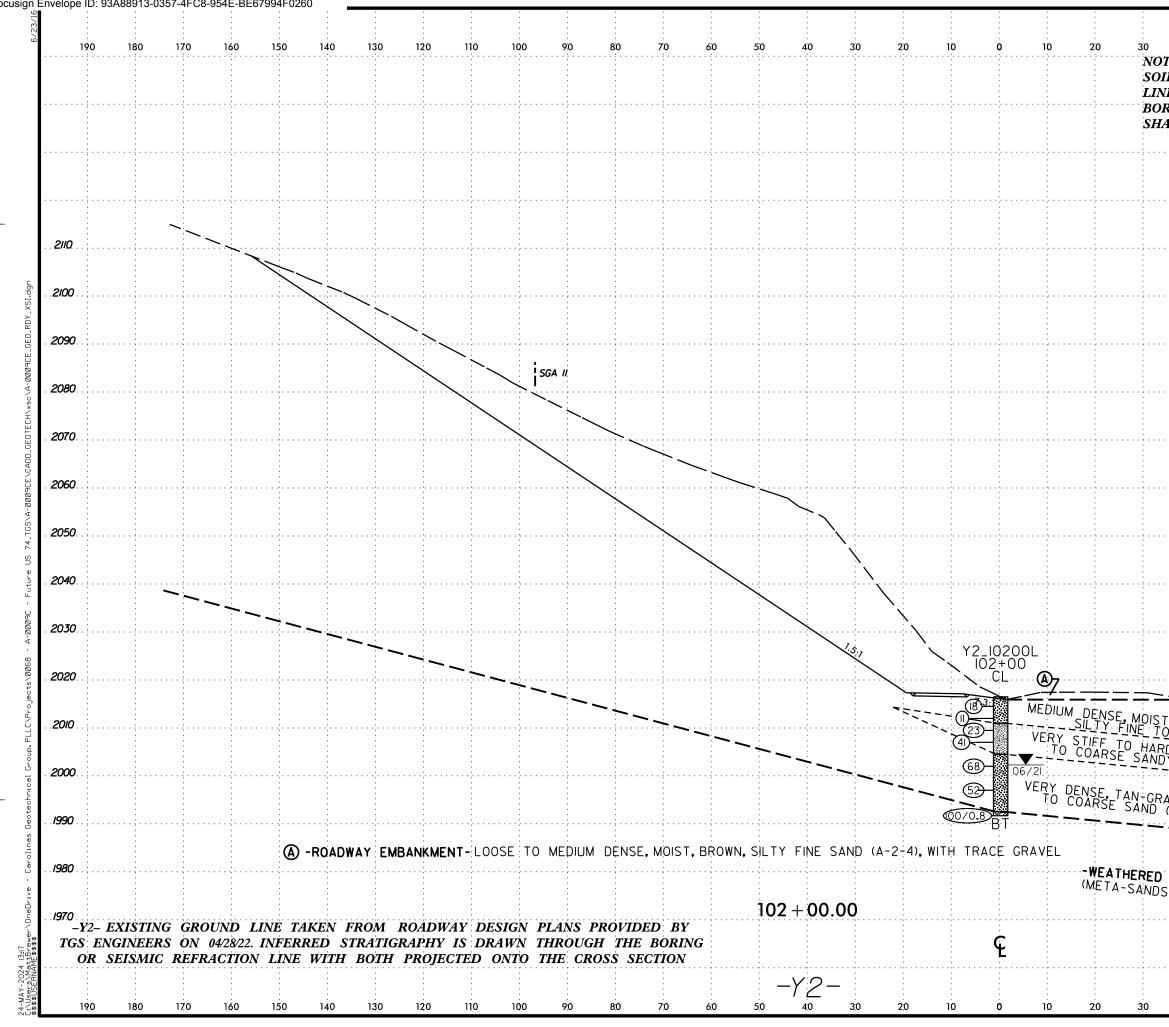


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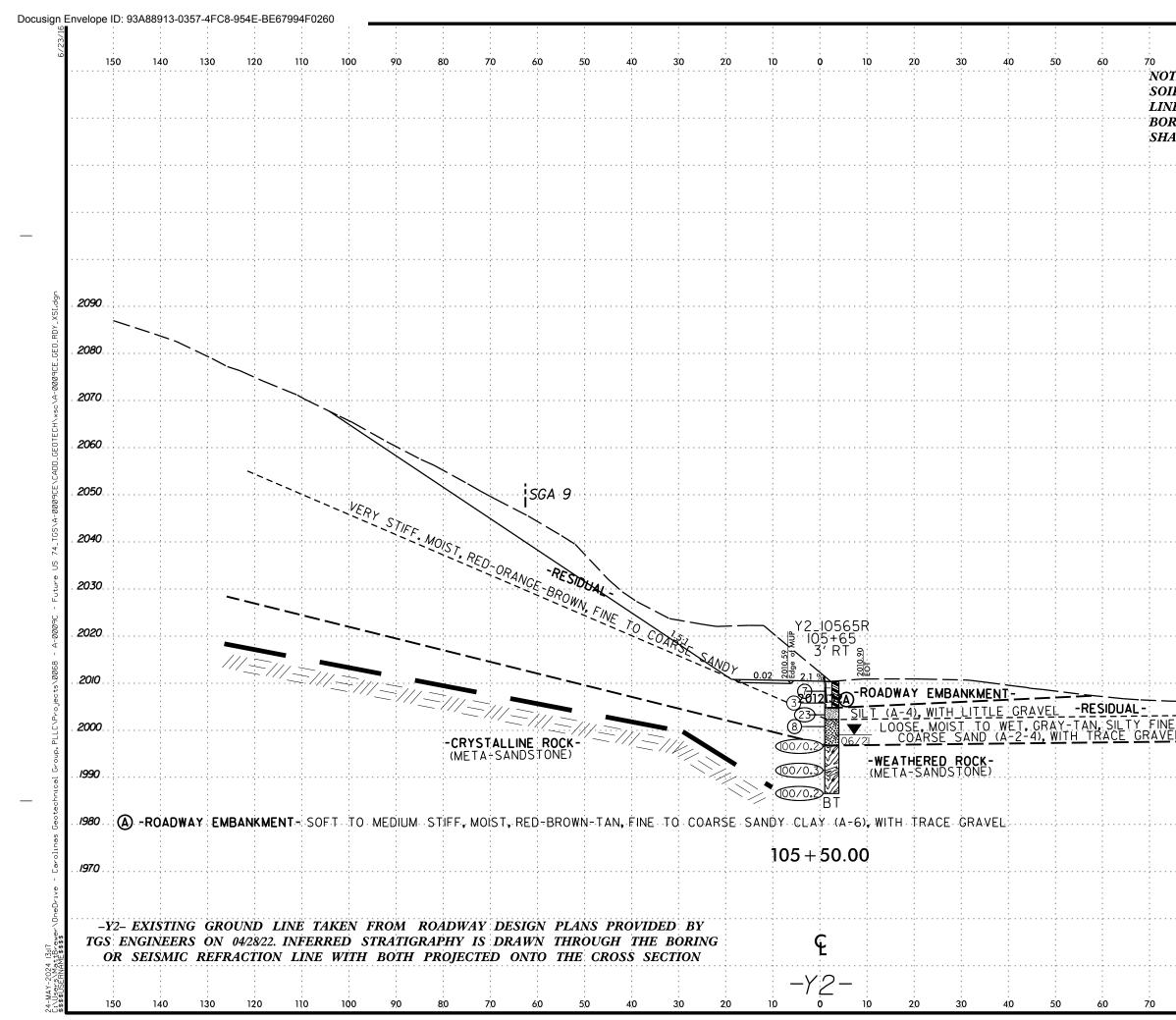




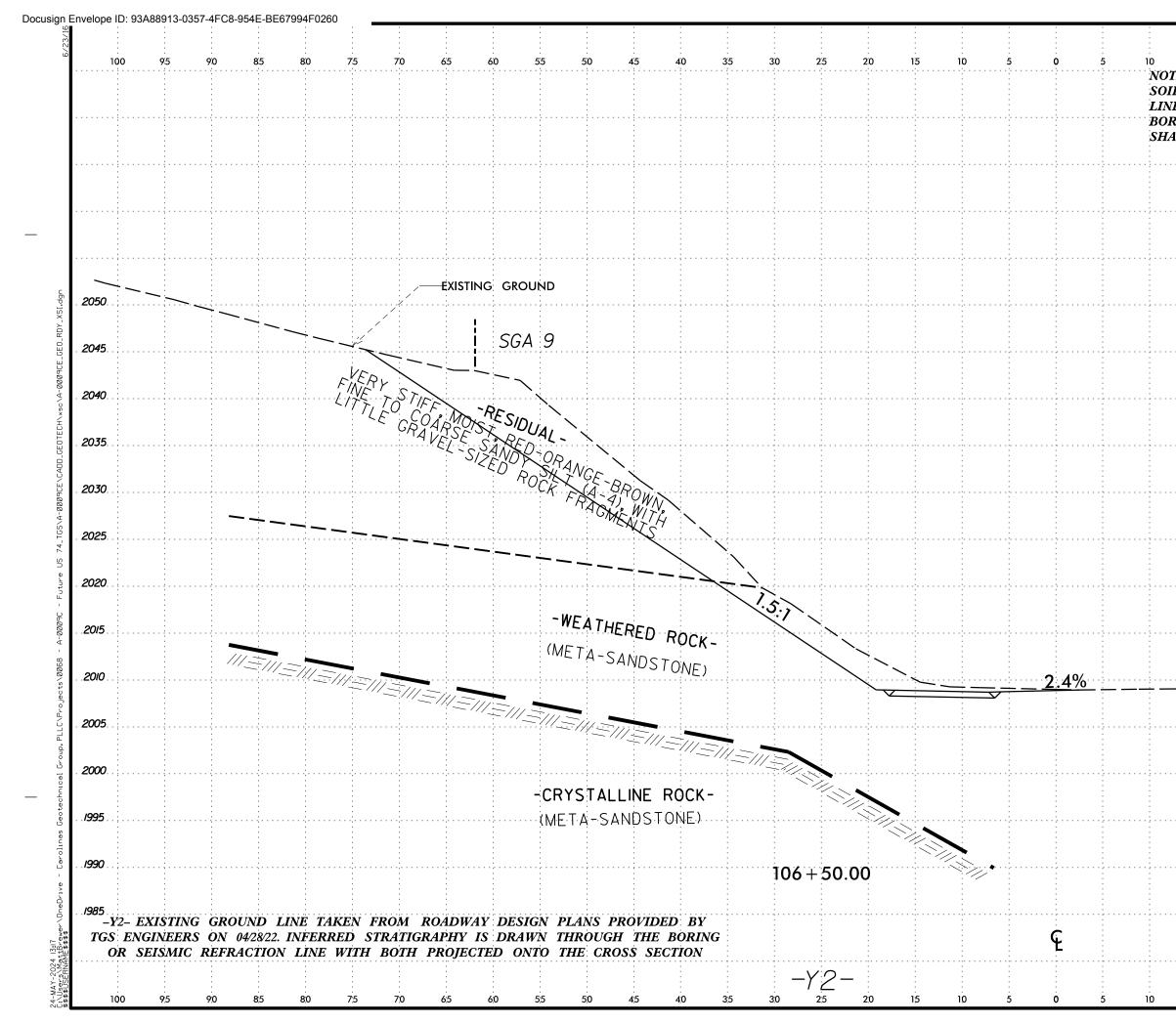
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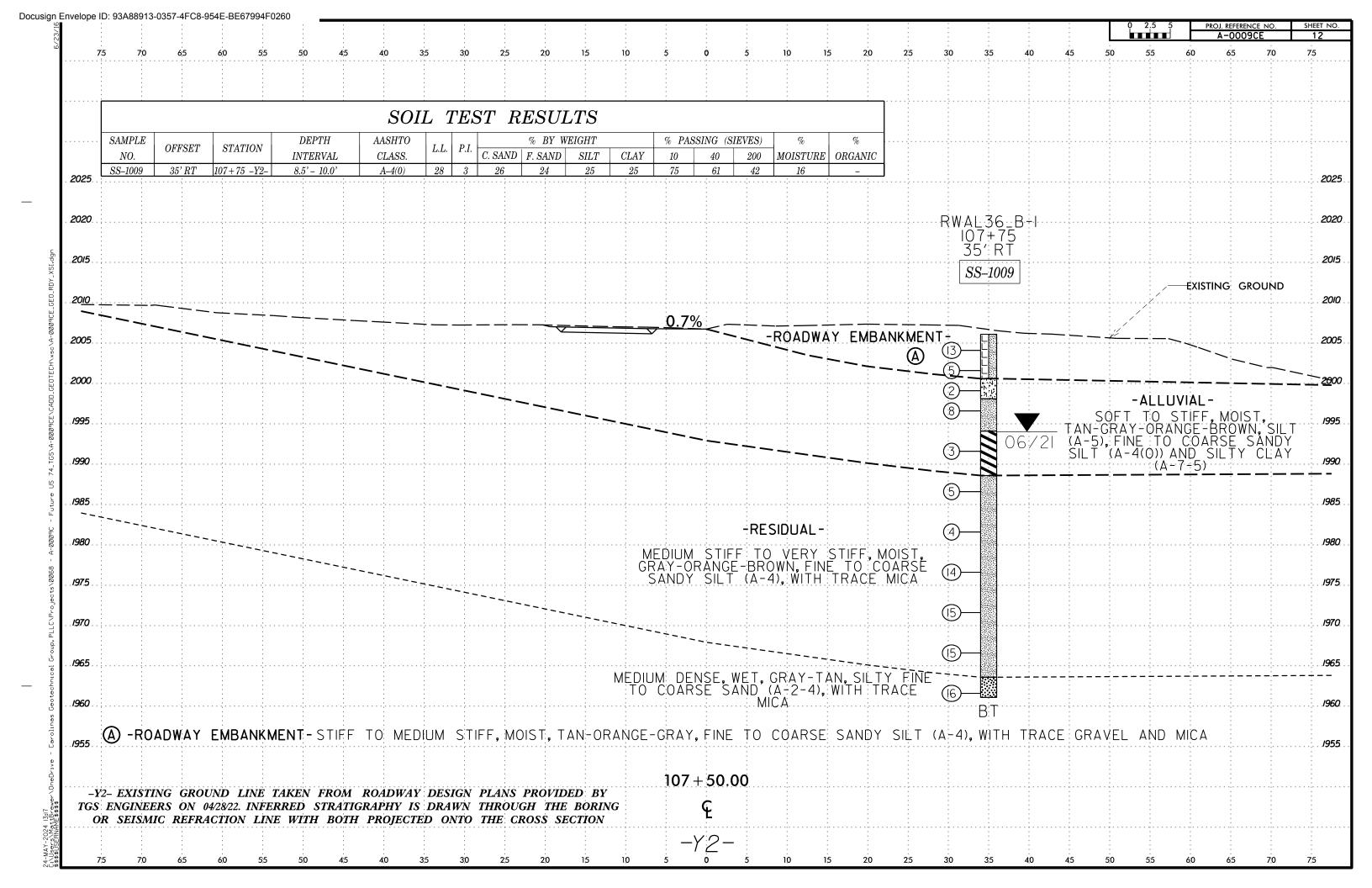
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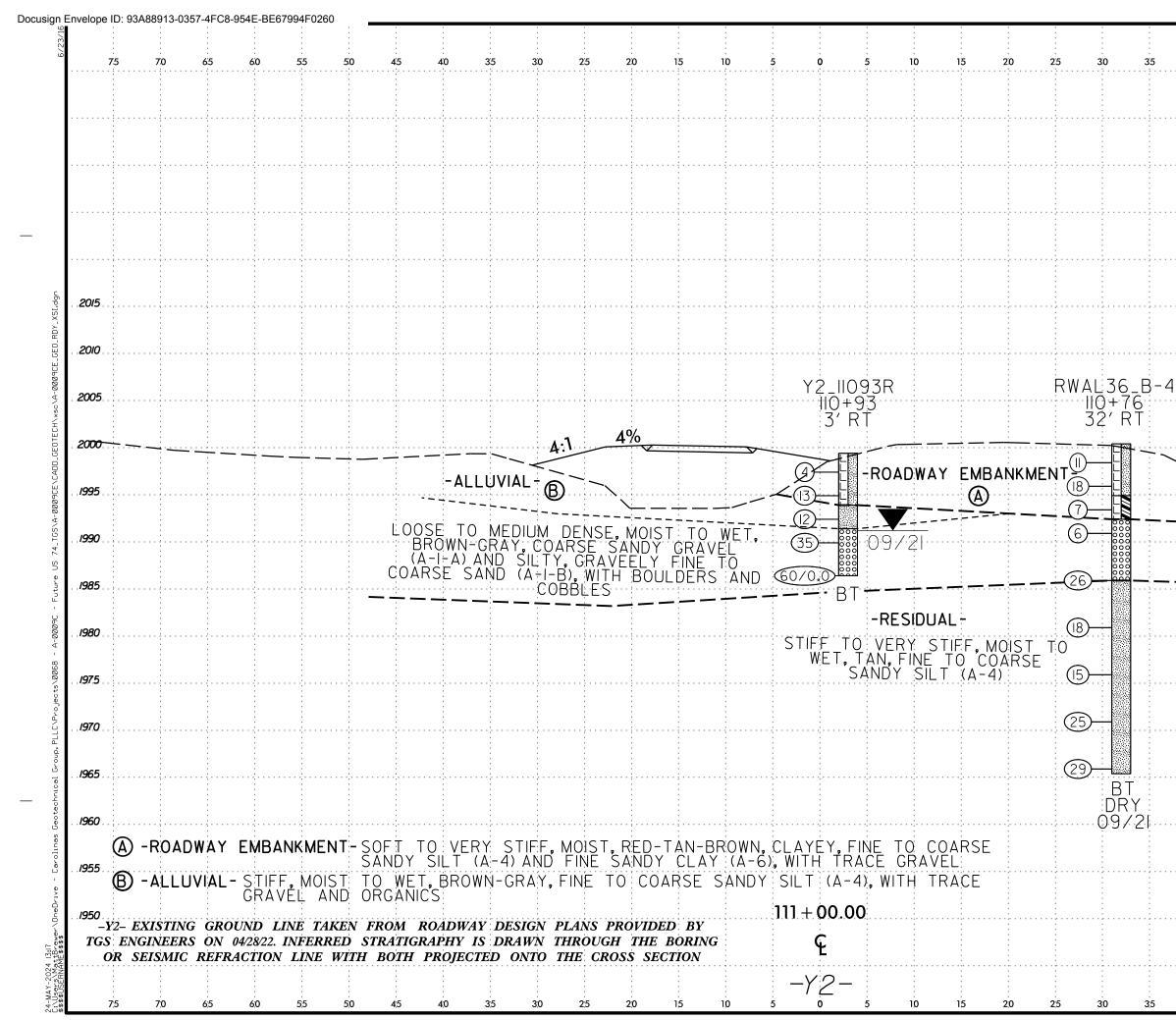
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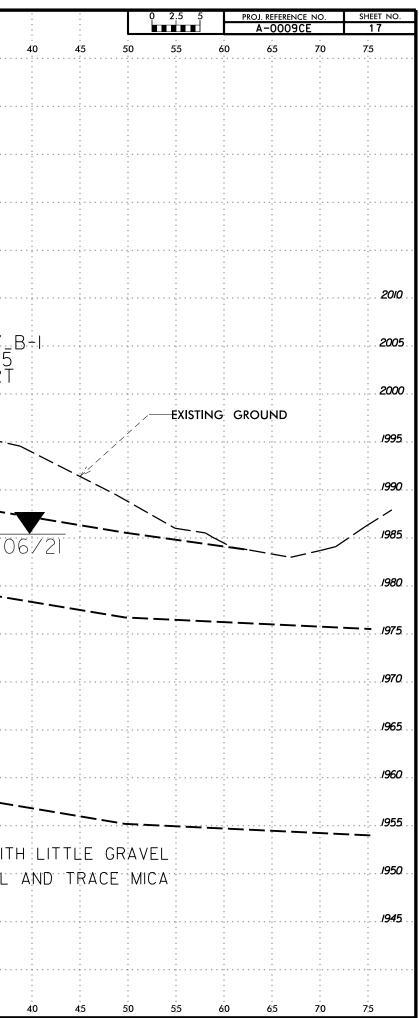
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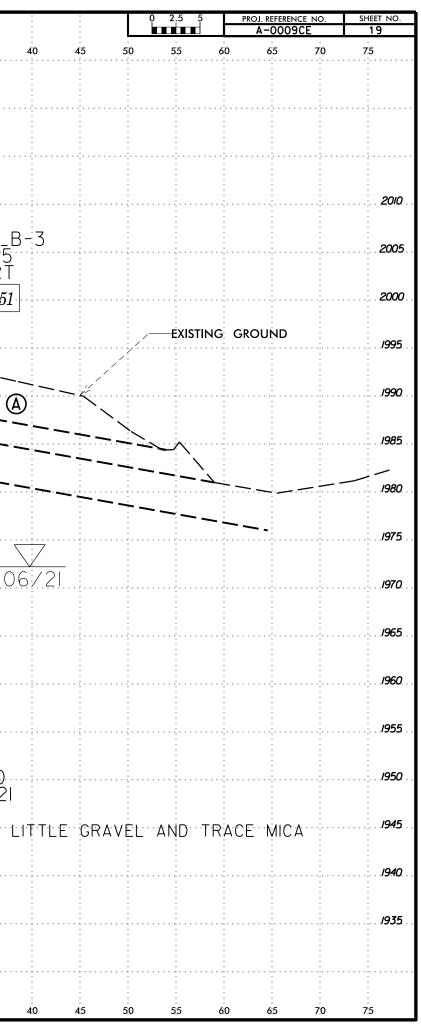
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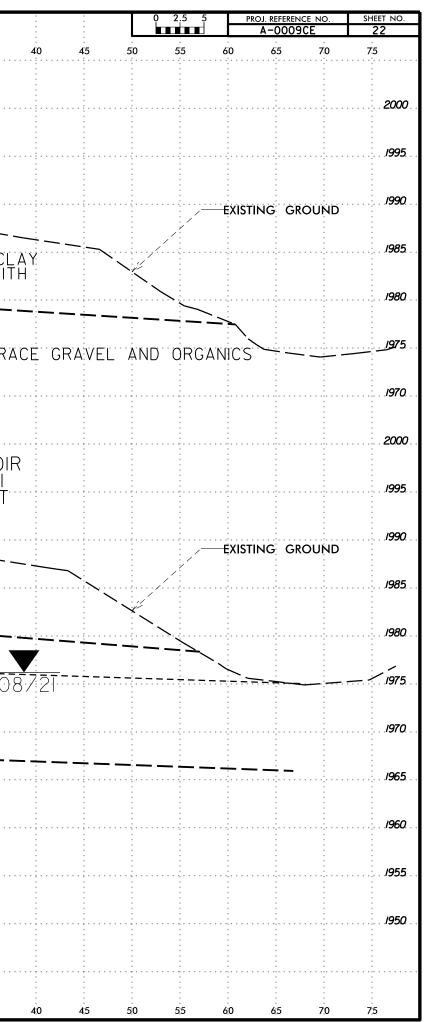
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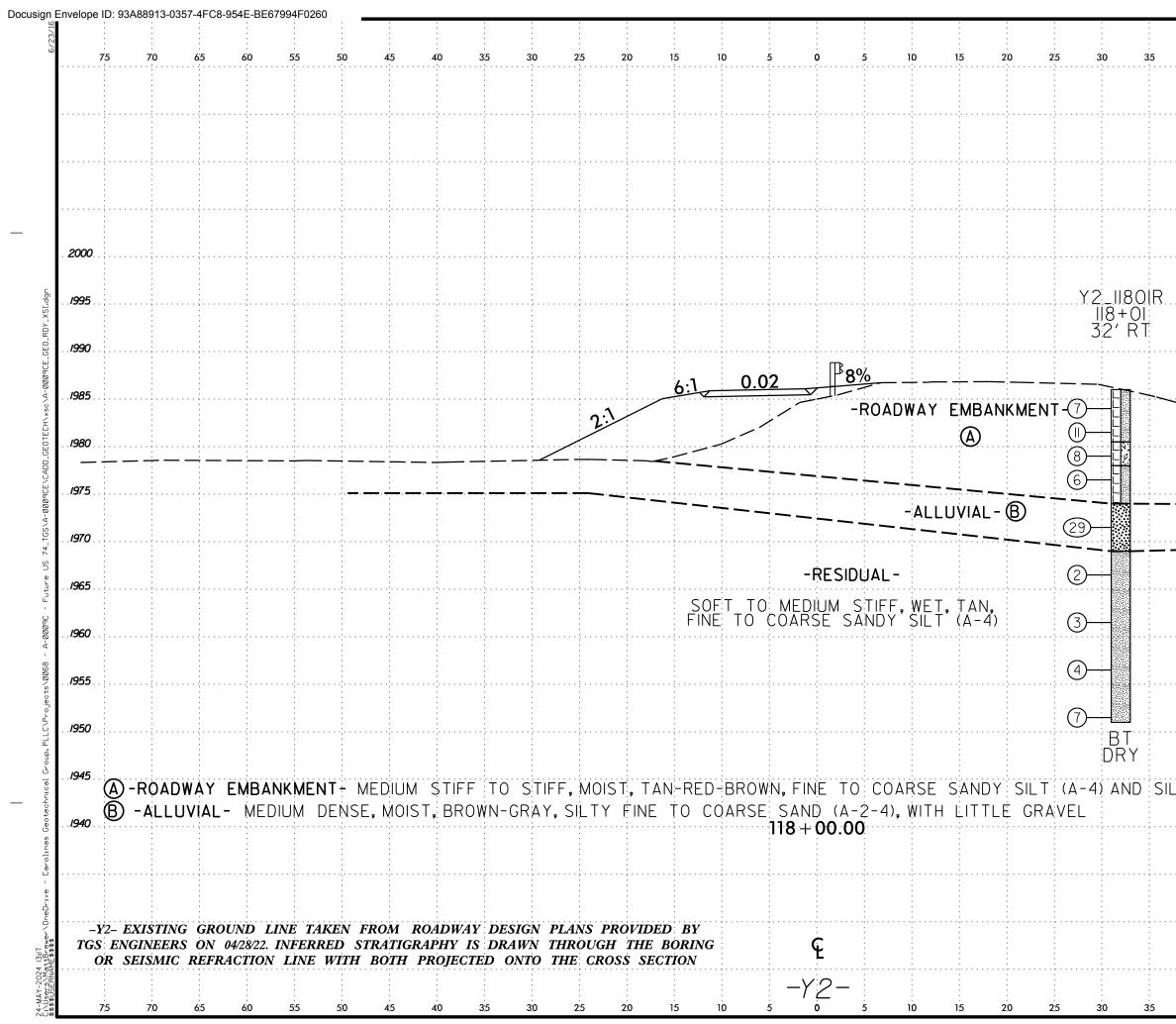
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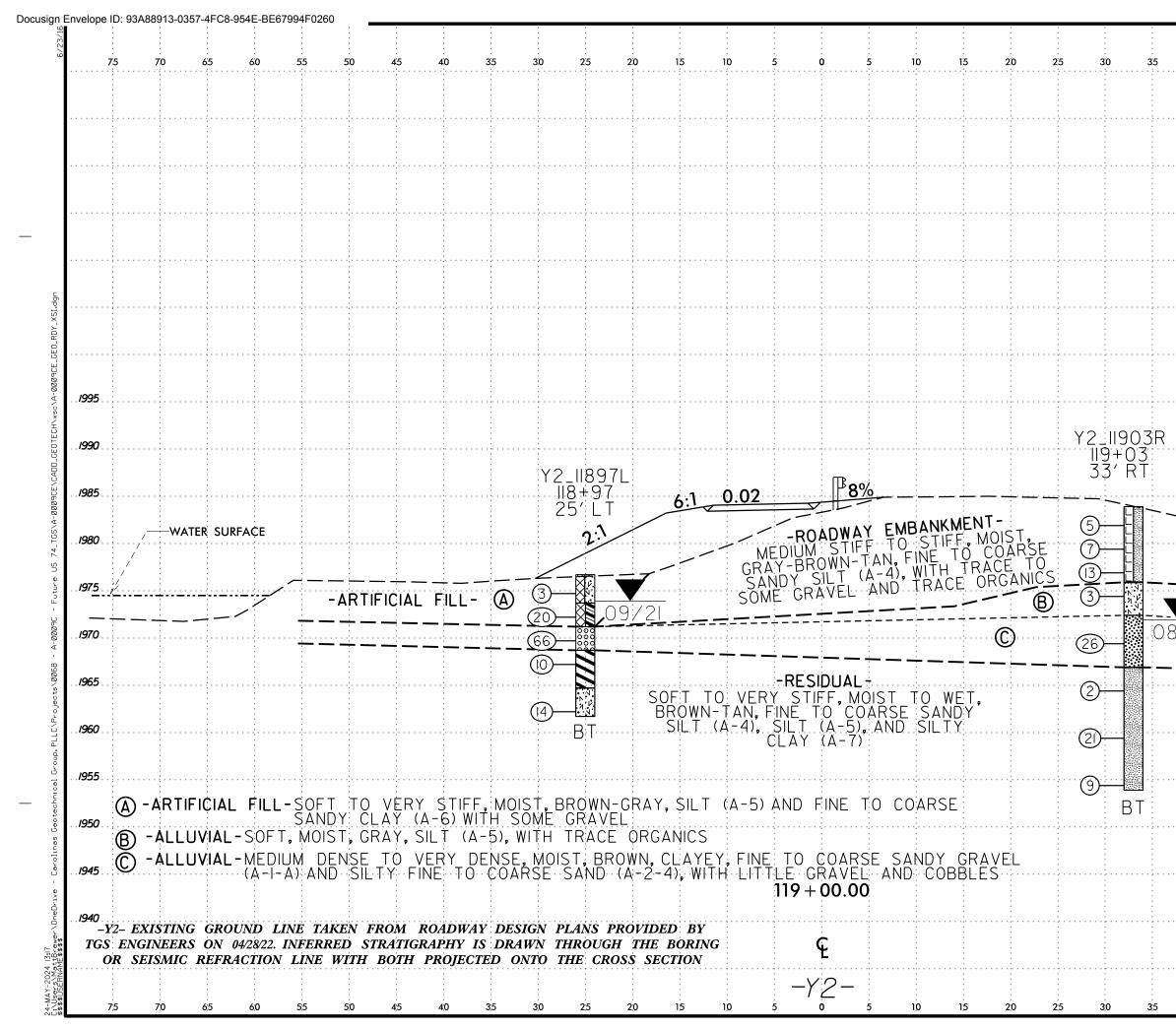




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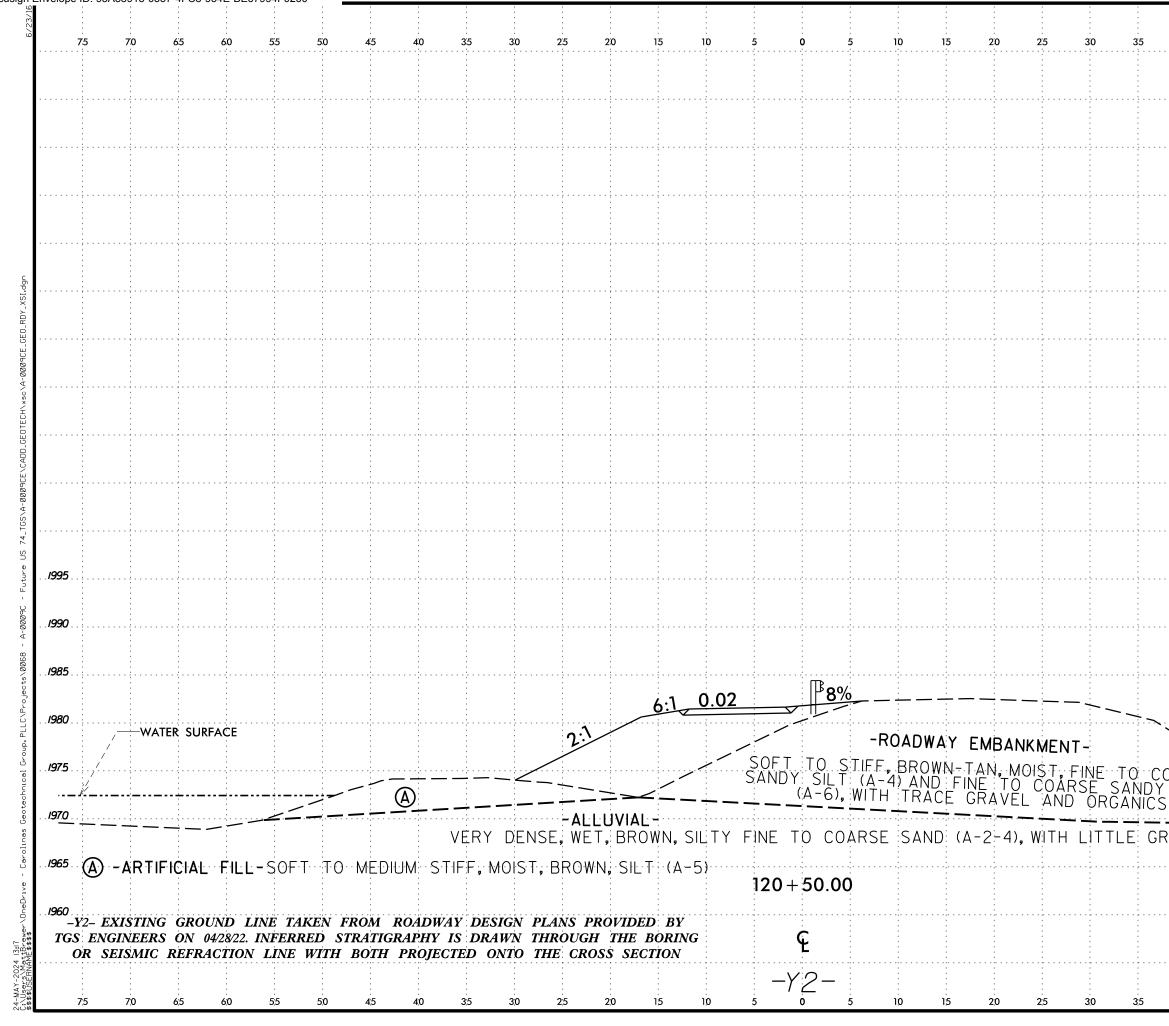
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⁶⁰ -Y2- EXISTING GROUND LINE TAKEN FROM ROADWAY DESIGN PLANS PROVIDED BY TGS ENGINEERS ON 04/28/22. INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORING OR SEISMIC REFRACTION LINE WITH BOTH PROJECTED ONTO THE CROSS SECTION $-\gamma 2 - \gamma$				-,		-ALL	UVIAL-SUFI	F, WU	ST, G	RAY, SILT (A-5	5), W11H	TRACE OR	GANICS			
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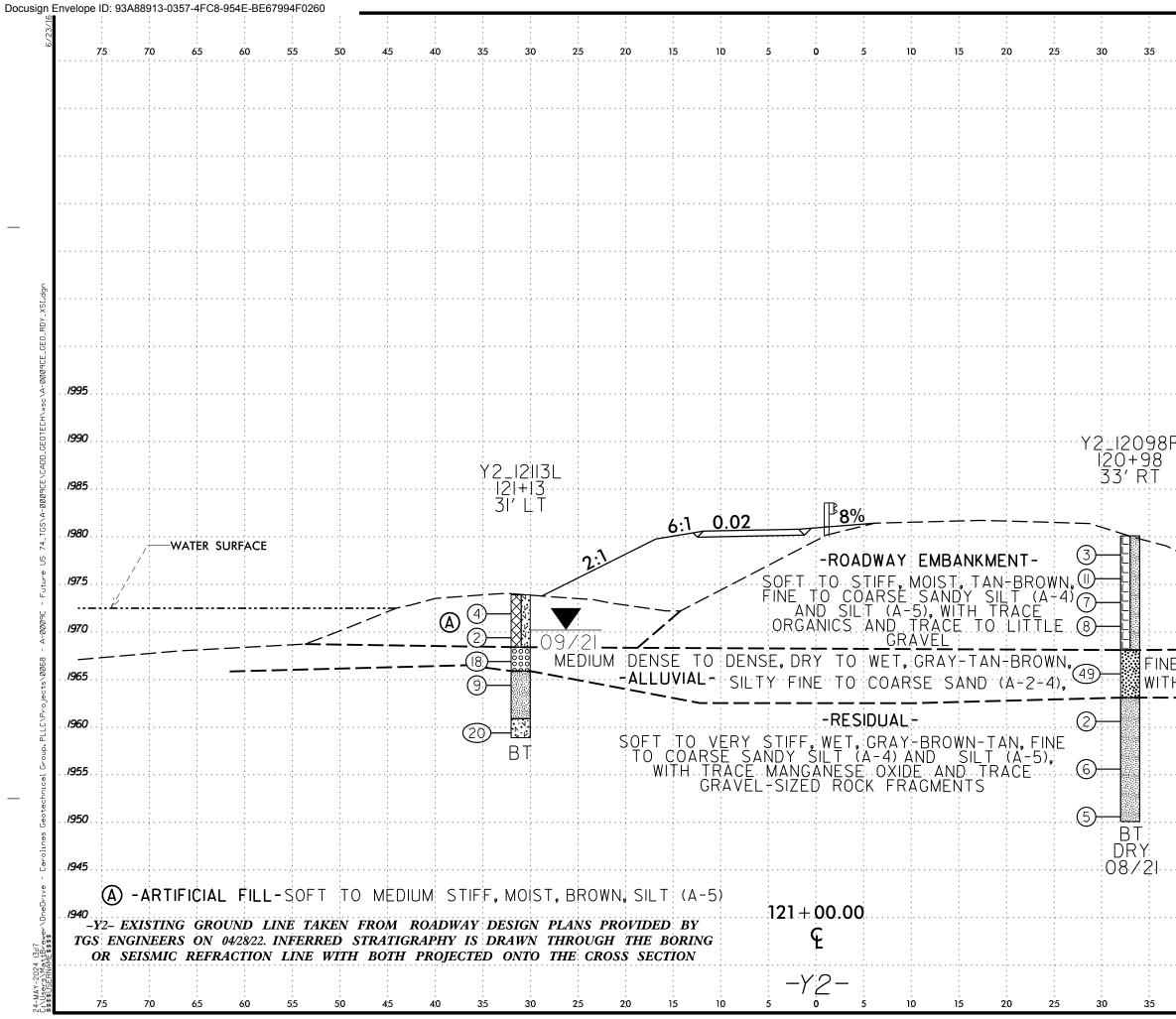
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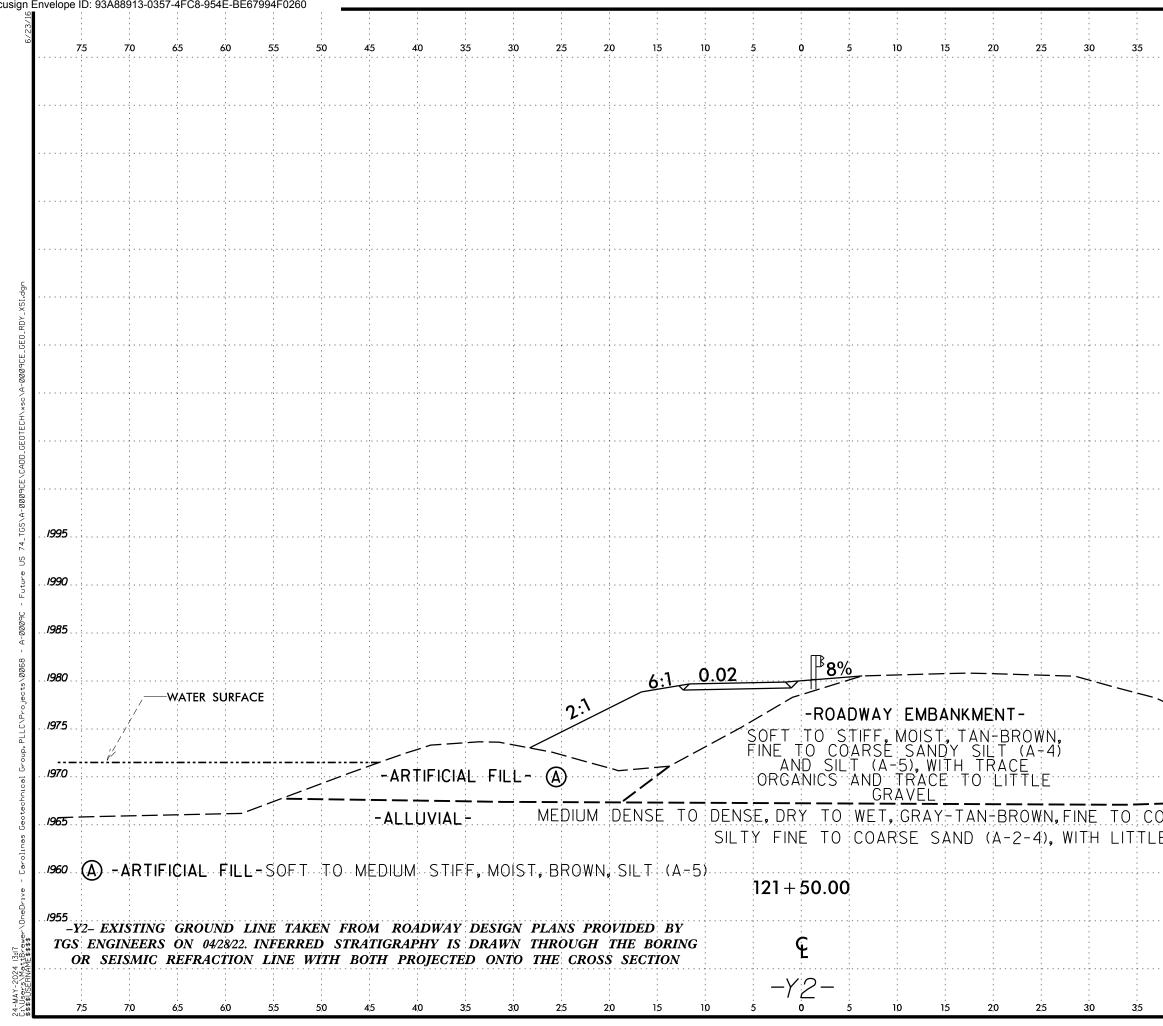
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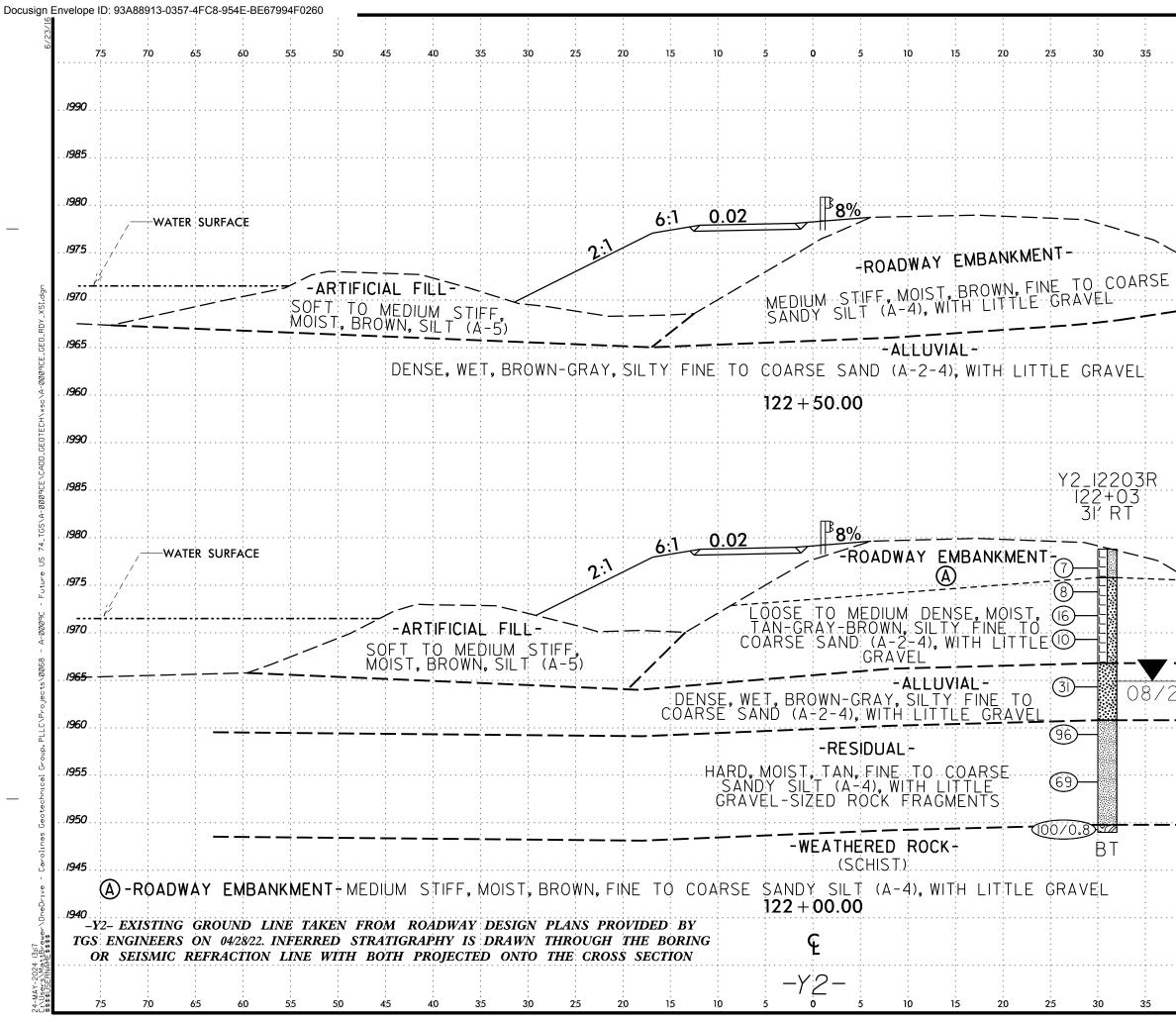
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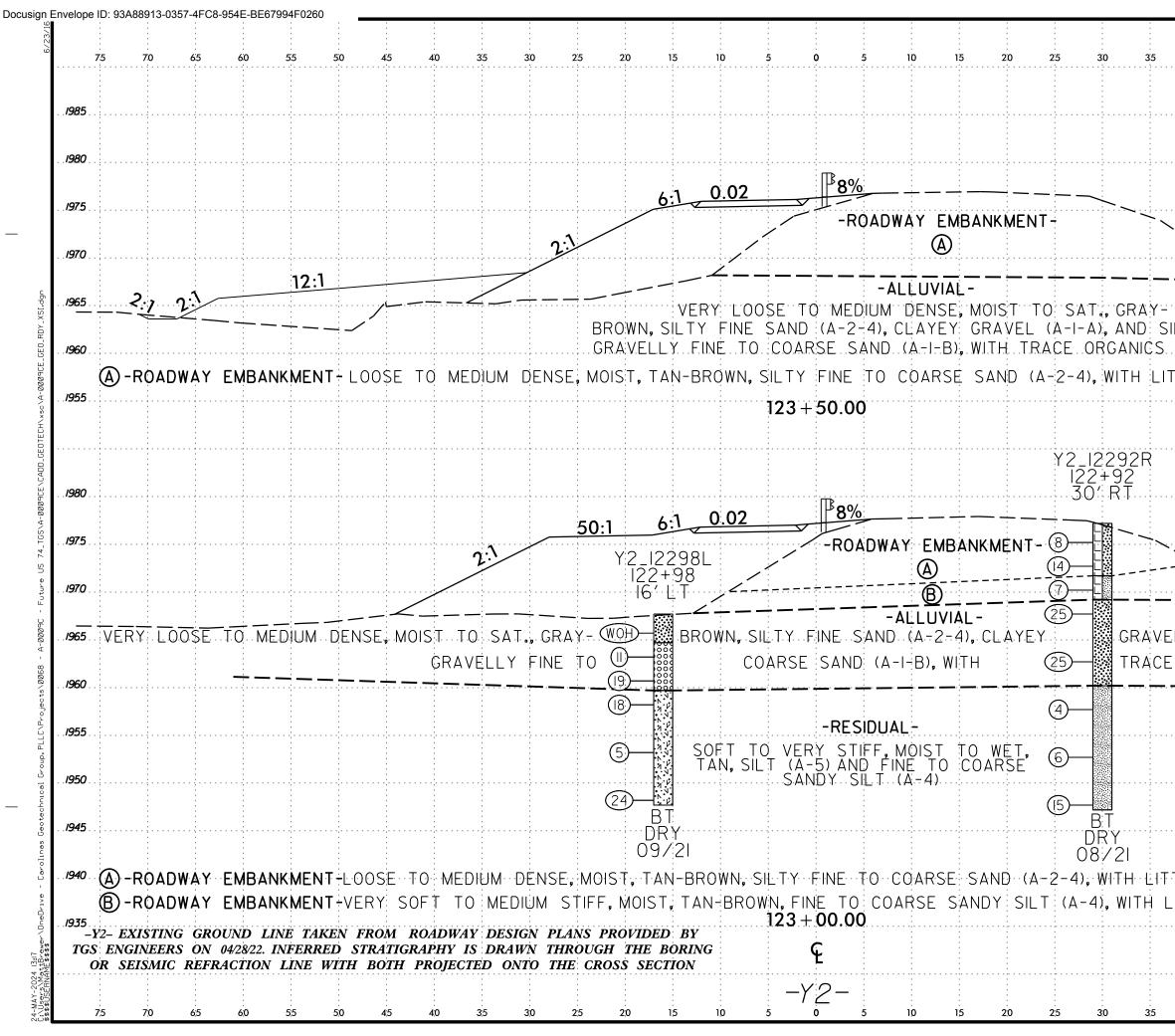
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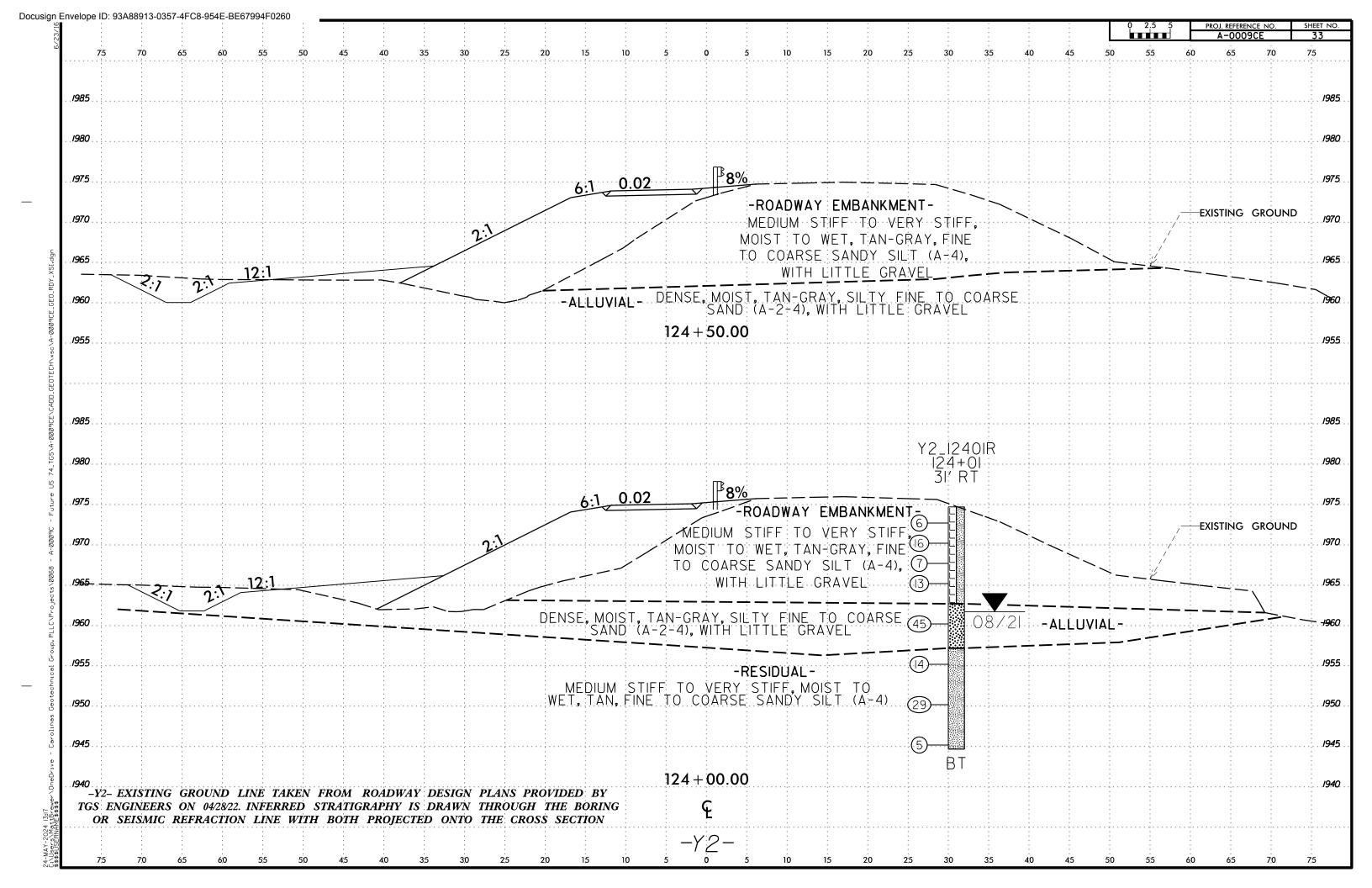
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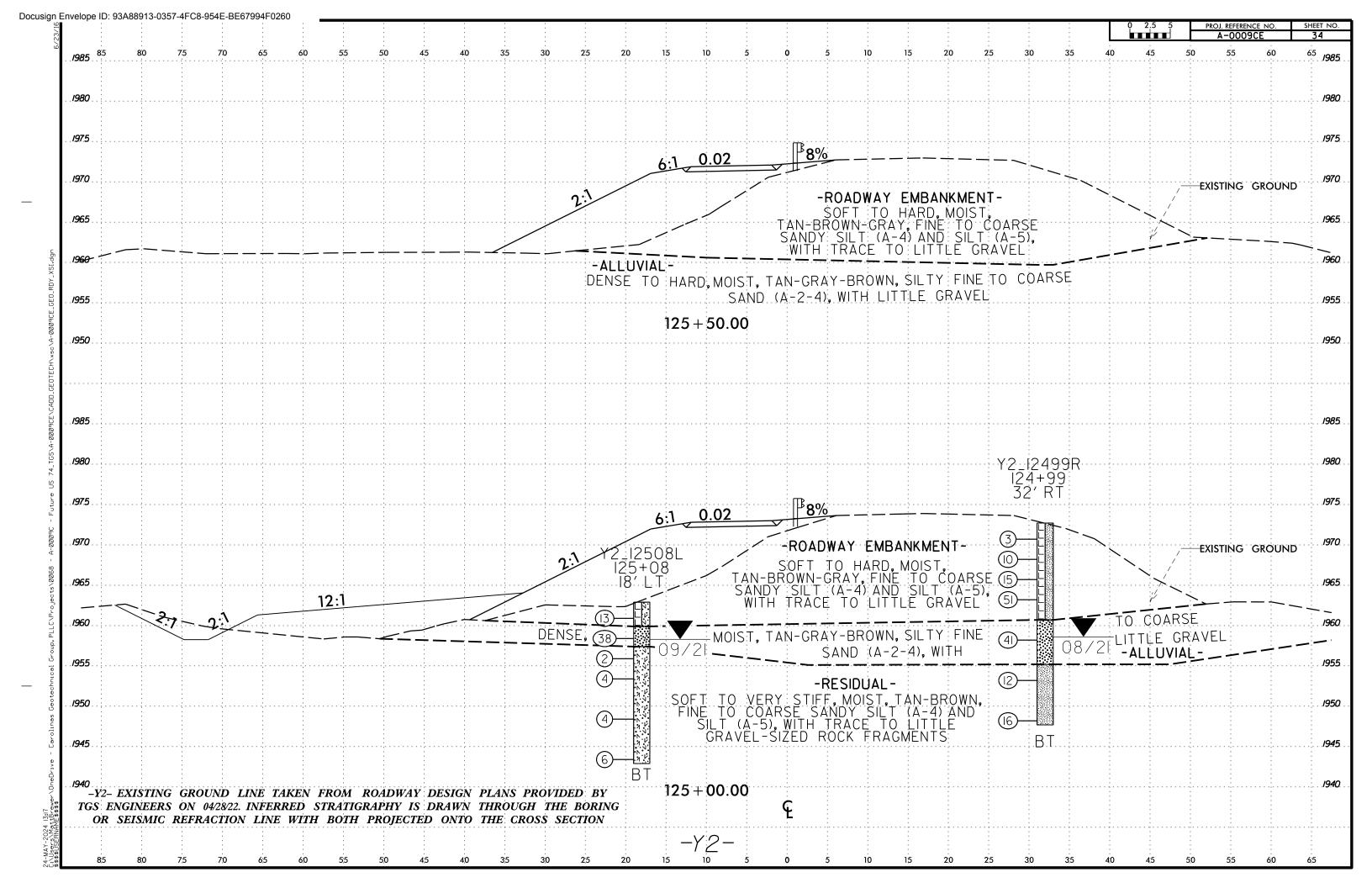


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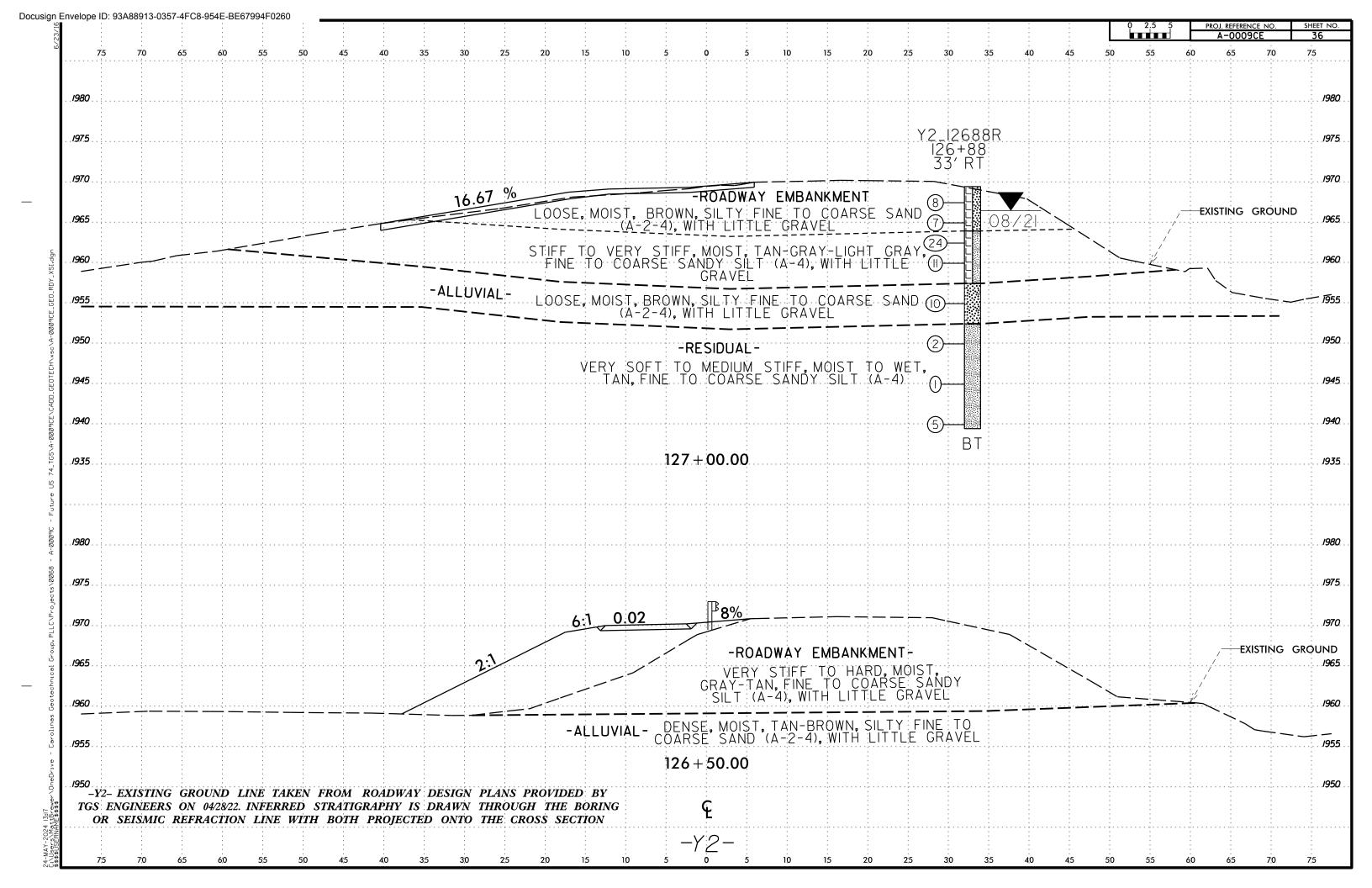
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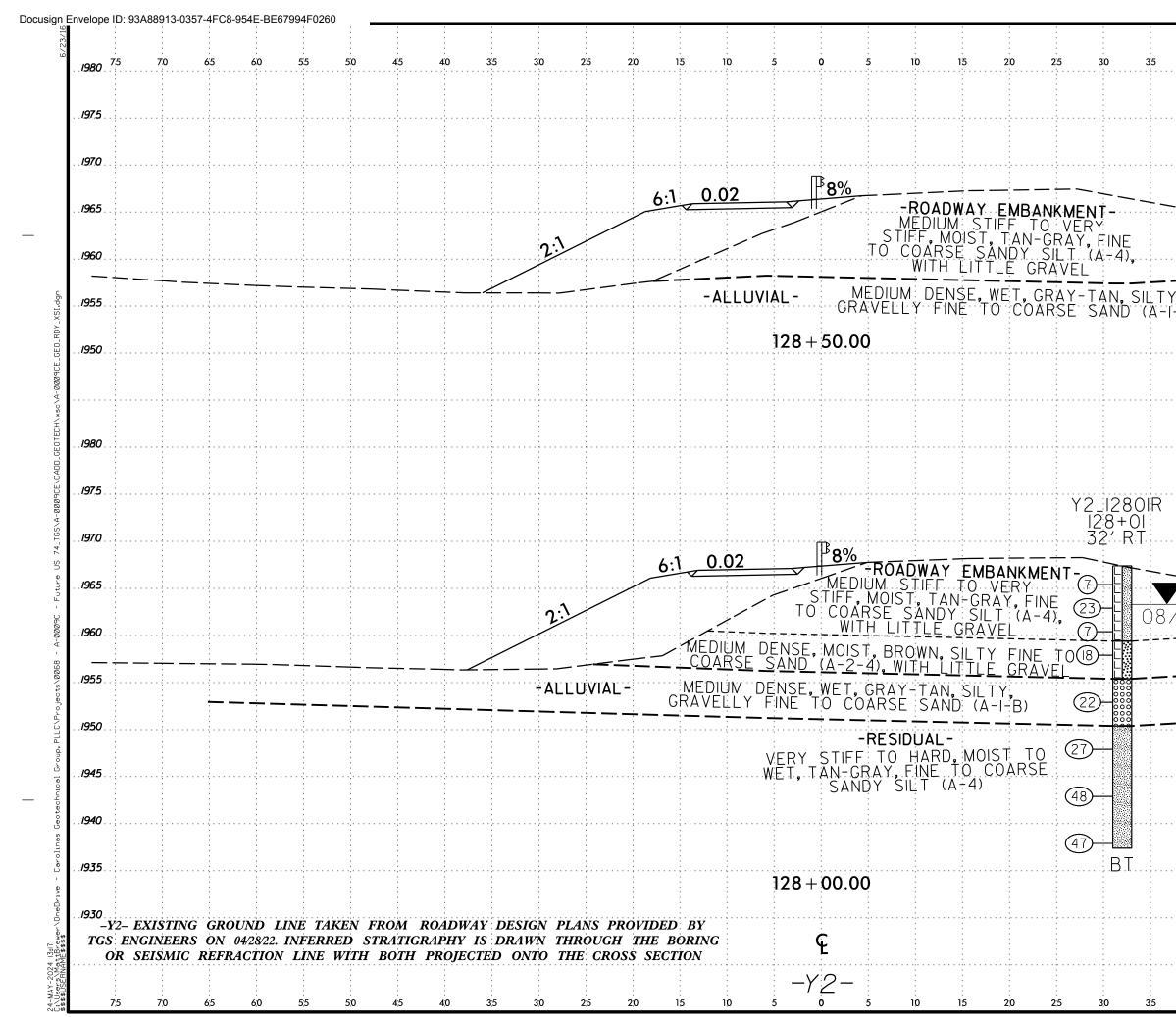
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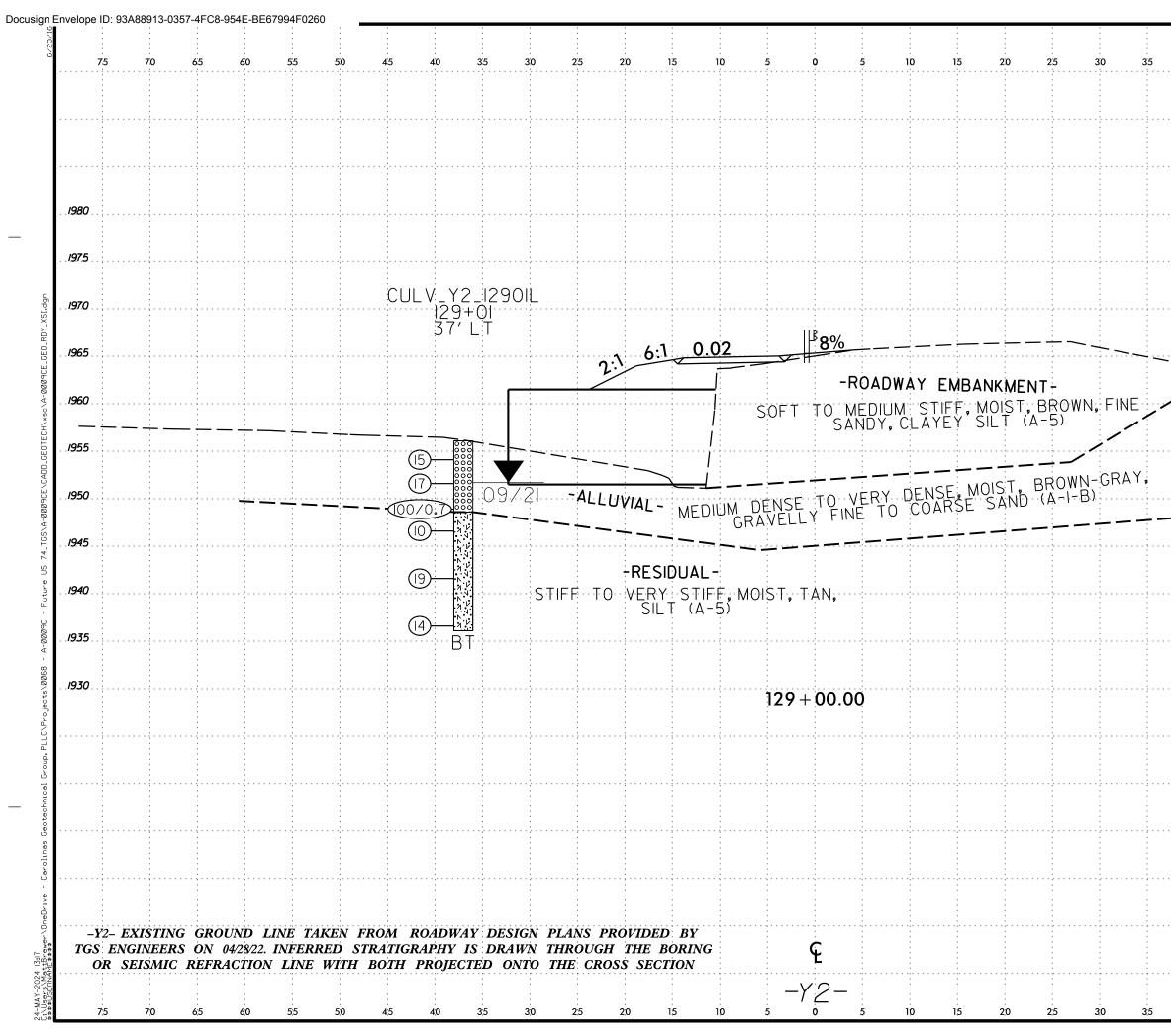


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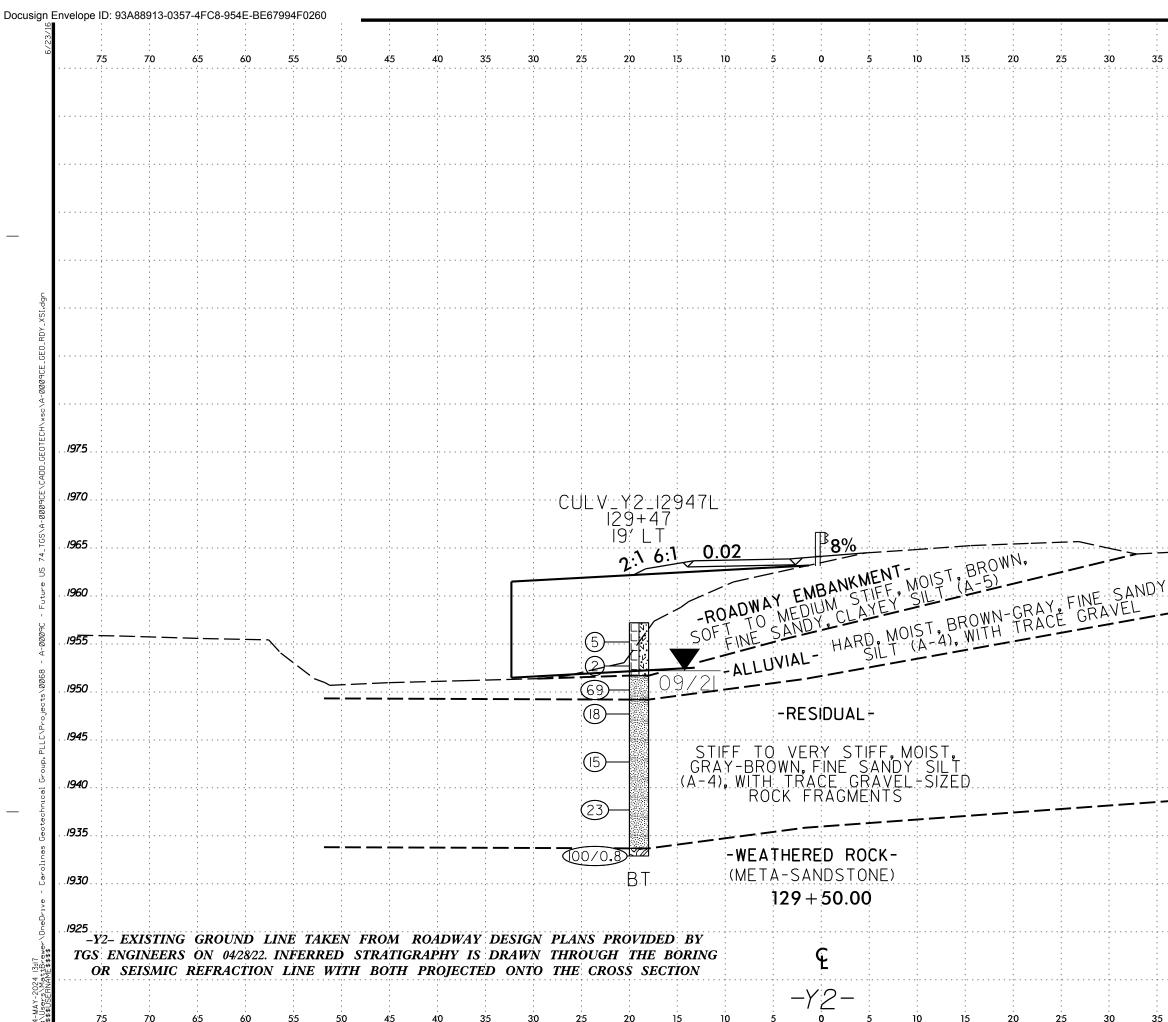
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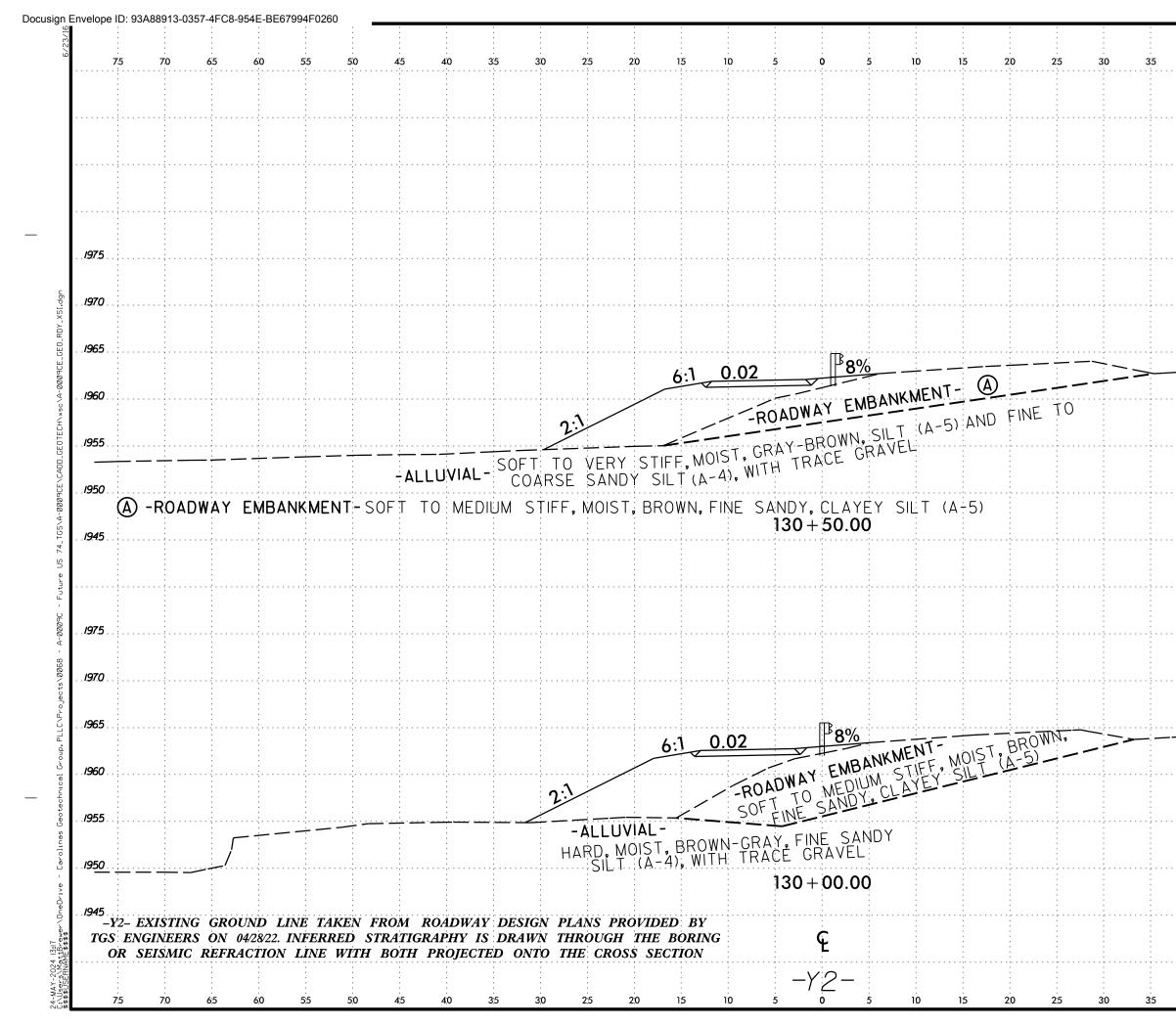
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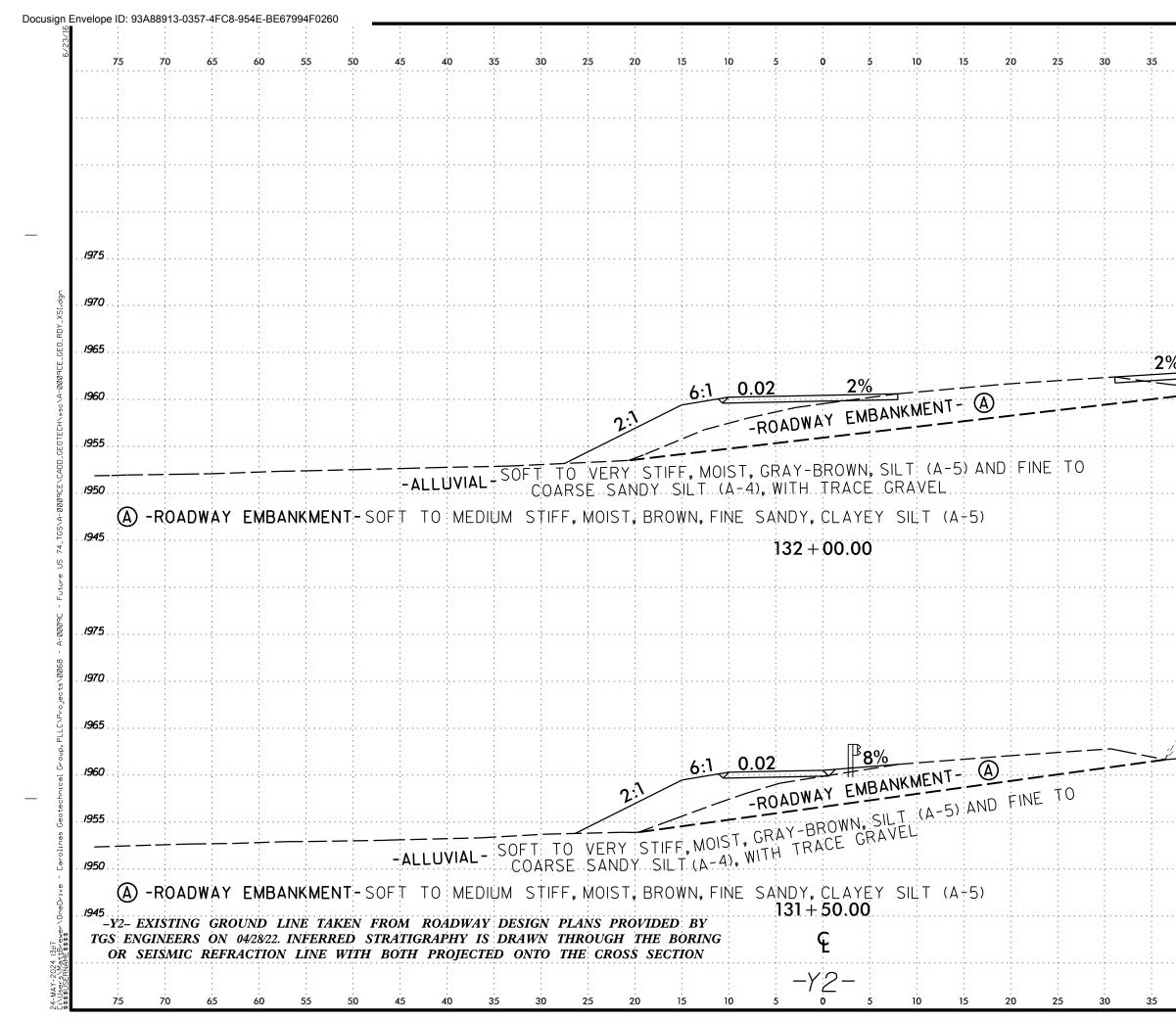
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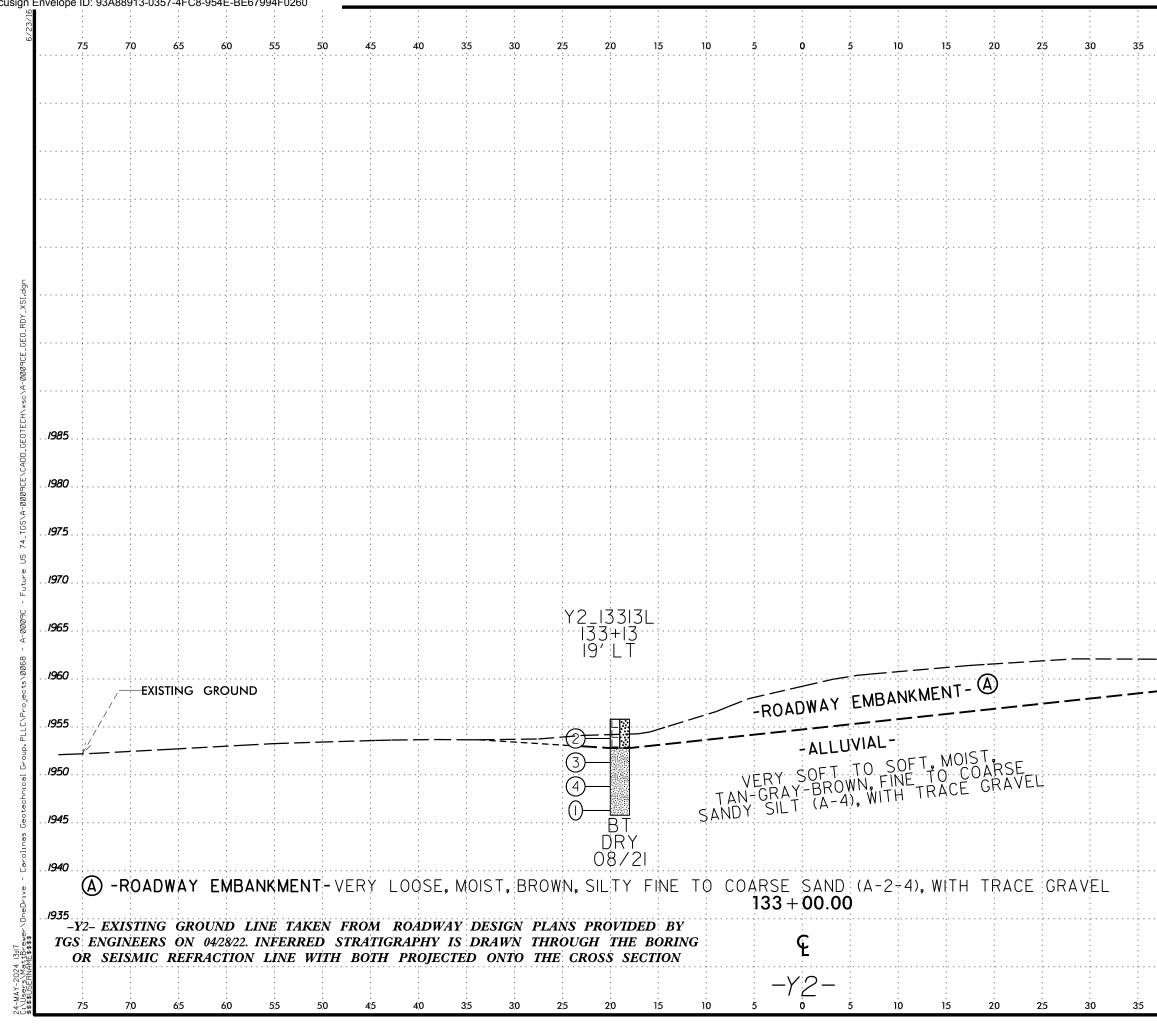
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# NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT SUBSURFACE INVESTIGATION APPENDIX A SOIL TEST RESULTS (I)

REFERENCE: A-0009CE

32572

**PROJECT:** 



SHEET NO.

# 47

Prepared in the Office of: FALCON ENGINEERS, INC CARY, NORTH CAROLINA NCDOT LAB CERT. NO. 105–0803

	SOIL	TEST	RESULTS
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SOIL TEST RESULTS															
SAMPLE	OFFSET STATION		DEPTH	AASHTO		P.I.		% BY WEIGHT			% PASSING (SIEVES)			%	%
NO.	OFFSEI	STATION	INTERVAL	CLASS.	L.L.		C. SAND	F. SAND	SILT	CLAY	10	40	200	MOISTURE	ORGANIC
SS-4483	38' LT	103+48 -Y2-	3.5' - 5.0'	A - 4(0)	28	2	32	25	24	19	96	74	49	14	_
SS-1009	35' RT	107+75 -Y2-	8.5' - 10.0'	A - 4(0)	28	3	26	24	25	25	75	61	42	16	_
SS-4451	35' RT	114+25 -Y2-	8.5' - 10.0'	A-4(1)	36	5	25	27	29	19	84	69	47	15	_

### PROJECT REFERENCE NO. A-0009CE

## 48

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION DIVISION OF HIGHWAYS GEOTECHNICAL ENGINEERING UNIT SUBSURFACE INVESTIGATION APPENDIX B

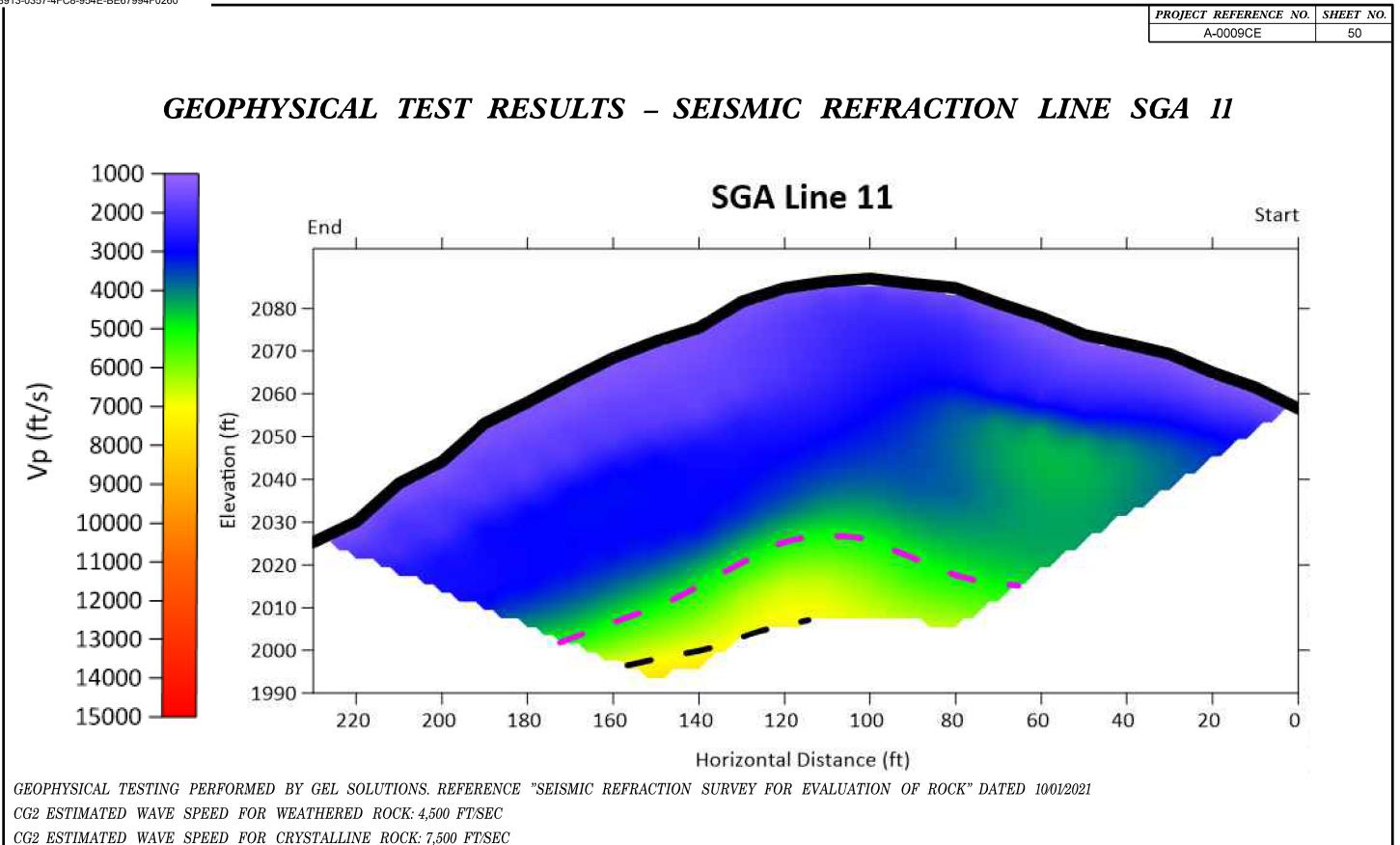
**GEOPHYSICAL TEST RESULTS** 

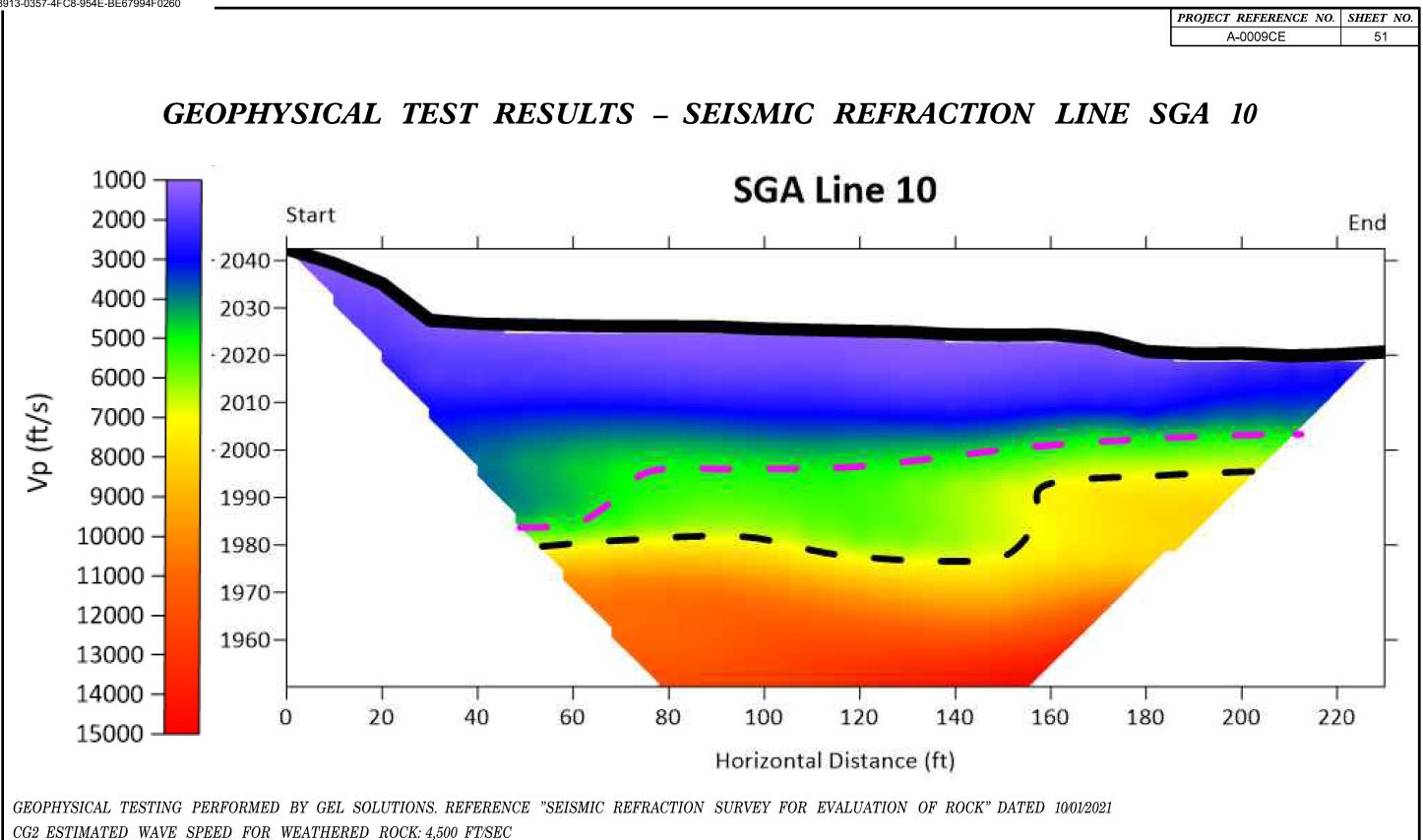
REFERENCE: A-0009CE

PROJECT: 32572



SHEET NO.





CG2 ESTIMATED WAVE SPEED FOR CRYSTALLINE ROCK: 7,500 FT/SEC

